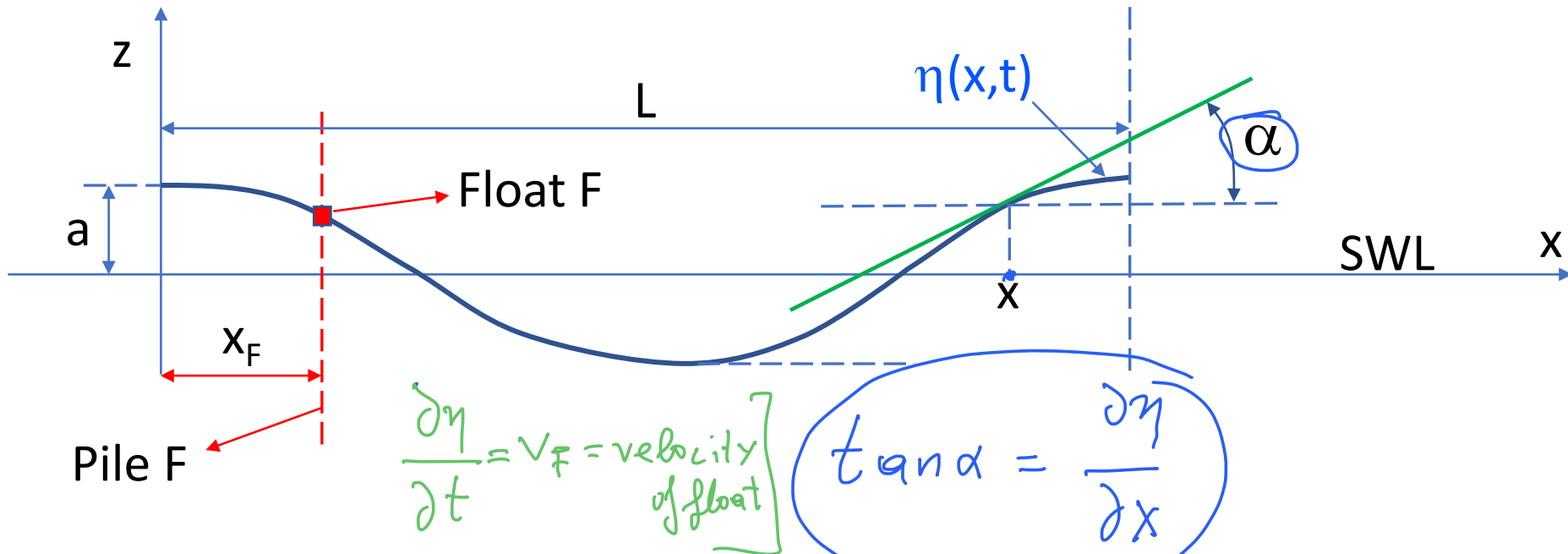


SLOPE OF WAVE



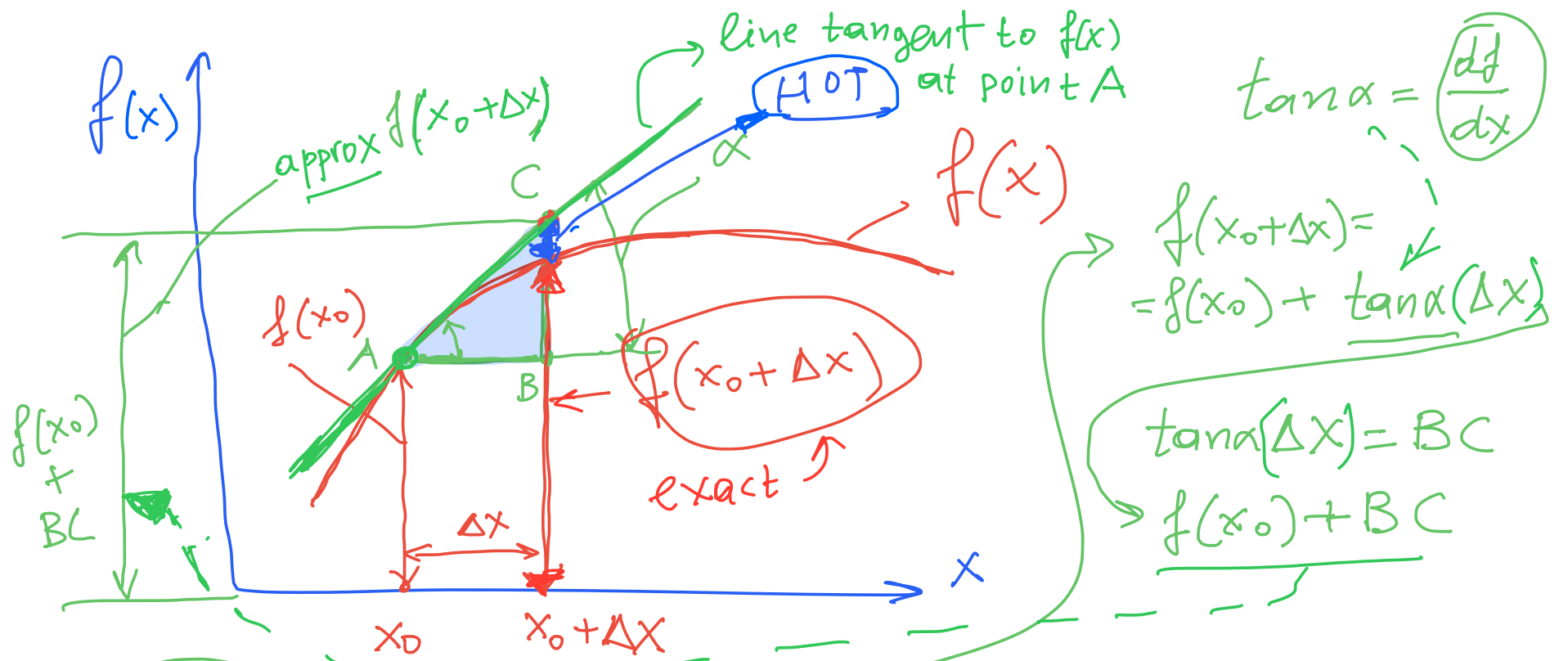
$$\eta(x, t) = a \cos(kx - \omega t)$$

$$\frac{\partial \eta}{\partial x} = a \left[-\sin(kx - \omega t) \right] k = -\underline{ak} \sin(kx - \omega t)$$

In general

max slope is ak

if: $f = A \underline{\cos}(kx \pm \omega t)$ or $A \underline{\sin}(kx \pm \omega t)$
max f : $|A|$ min f : $-|A|$



Taylor expansion:

$$f(x_0 + \Delta x) = f(x_0) + \frac{df}{dx} \Big|_{x=x_0} \Delta x + \frac{d^2 f}{dx^2} \Big|_{x=x_0} \frac{\Delta x^2}{2!} + \frac{d^3 f}{dx^3} \Big|_{x=x_0} \frac{\Delta x^3}{3!} + \dots$$

If: $\Delta x = 0.1 \rightarrow \Delta x^2 = 0.01 \rightarrow \Delta x^3 = 0.001$

Linear Taylor expansion

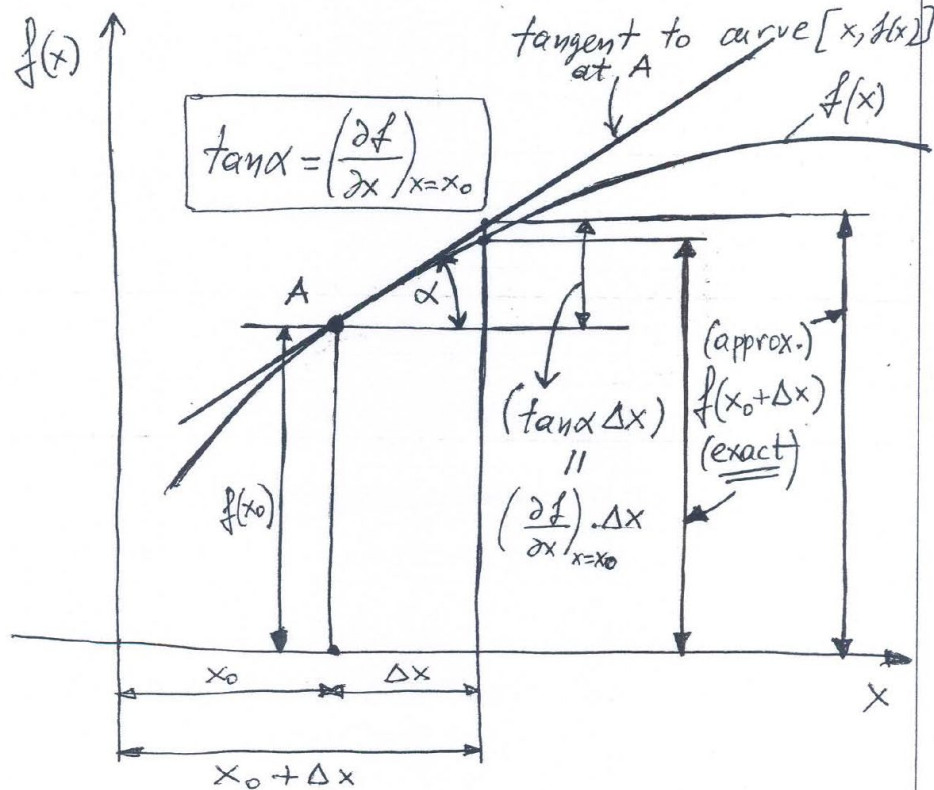
$$f(x_0 + \Delta x) \approx f(x_0) + \frac{df}{dx} \Delta x$$

Higher Order **HOT**

Terms can be ignored for small Δx

PHYSICAL MEANING OF 1ST ORDER APPROXIMATION

$$f(x_0 + \Delta x) \approx f(x_0) + \left(\frac{\partial f}{\partial x} \right)_{x=x_0} \cdot \Delta x$$



Taylor expansion:

$$f(x_0 + \Delta x) = f(x_0) + f'(x_0) \frac{\Delta x}{1!} + f''(x_0) \frac{(\Delta x)^2}{2!} + f'''(x_0) \frac{(\Delta x)^3}{3!} + \dots$$

EXAMPLE ON 1st ORDER APPROXIMATION

Provide an approximation (first order expansion) of the following expression, H , for small values of α . Then apply the formula for $\alpha = 0.1$ and compare the answer to the exact value. Determine the percentage error: $(H_{approx} - H_{exact})/H_{exact} = ?$

α

α

$$H = \sqrt{1 + \alpha} = ?$$

(1)

$$f(x_0 + \Delta x) = f(x_0) + \frac{df}{dx} \Delta x$$

$$\downarrow$$

$$\textcircled{1}$$

$$\downarrow$$

$$\textcircled{\alpha}$$

$$\frac{d}{dx} x^b = b x^{b-1}$$

$$f(x) = \sqrt{x}$$

$$\sqrt{1 + \alpha}$$

$$= \sqrt{1}$$

$$+ \frac{df}{dx} \cdot \alpha$$

$$\textcircled{\alpha}$$

$$= 1 + \frac{\alpha}{2}$$

$$\rightarrow \frac{df}{dx} = \frac{d}{dx} \sqrt{x} = \frac{d}{dx} x^{1/2} = \frac{1}{2} x^{1/2 - 1} = \frac{1}{2} x^{-1/2} = \frac{1}{2\sqrt{x}}$$

$$\left. \frac{df}{dx} \right|_{x=1} = \frac{1}{2}$$

EXAMPLE ON 1ST ORDER APPROXIMATION

Provide an *approximation* (first order expansion) of the following expression, H , for *small* values of a . Then apply the formula for $a = 0.1$ and compare the answer to the exact value. Determine the percentage error: $(H_{\text{approx}} - H_{\text{exact}})/H_{\text{exact}} = ?$

$$H = \sqrt{1 + \alpha} = ? \quad (1)$$

$$\sqrt{1 + \alpha} \approx 1 + \frac{\alpha}{2}$$

Try $\alpha = 0.1$ $\sqrt{1 + \alpha} \approx 1 + \frac{0.1}{2} = 1.05 = H_{\text{approx}}$

$H_{\text{exact}} \sqrt{1 + \alpha} = 1.0488$

$$\% \text{ error} = \frac{H_{\text{approx}} - H_{\text{exact}}}{H_{\text{exact}}} = \frac{1.05 - 1.0488}{1.0488} = 0.00114 = 0.11\%$$

The above result can be generalized (using Taylor exp.) to the binomial approximations

$$(1 + \alpha)^r \approx 1 + r\alpha$$

$|\alpha| \ll 1$; r can be any real number

special case ($r = -1$)

$$\frac{1}{1 + \alpha}$$

$$= (1 + \alpha)^{-1} = 1 - \alpha$$

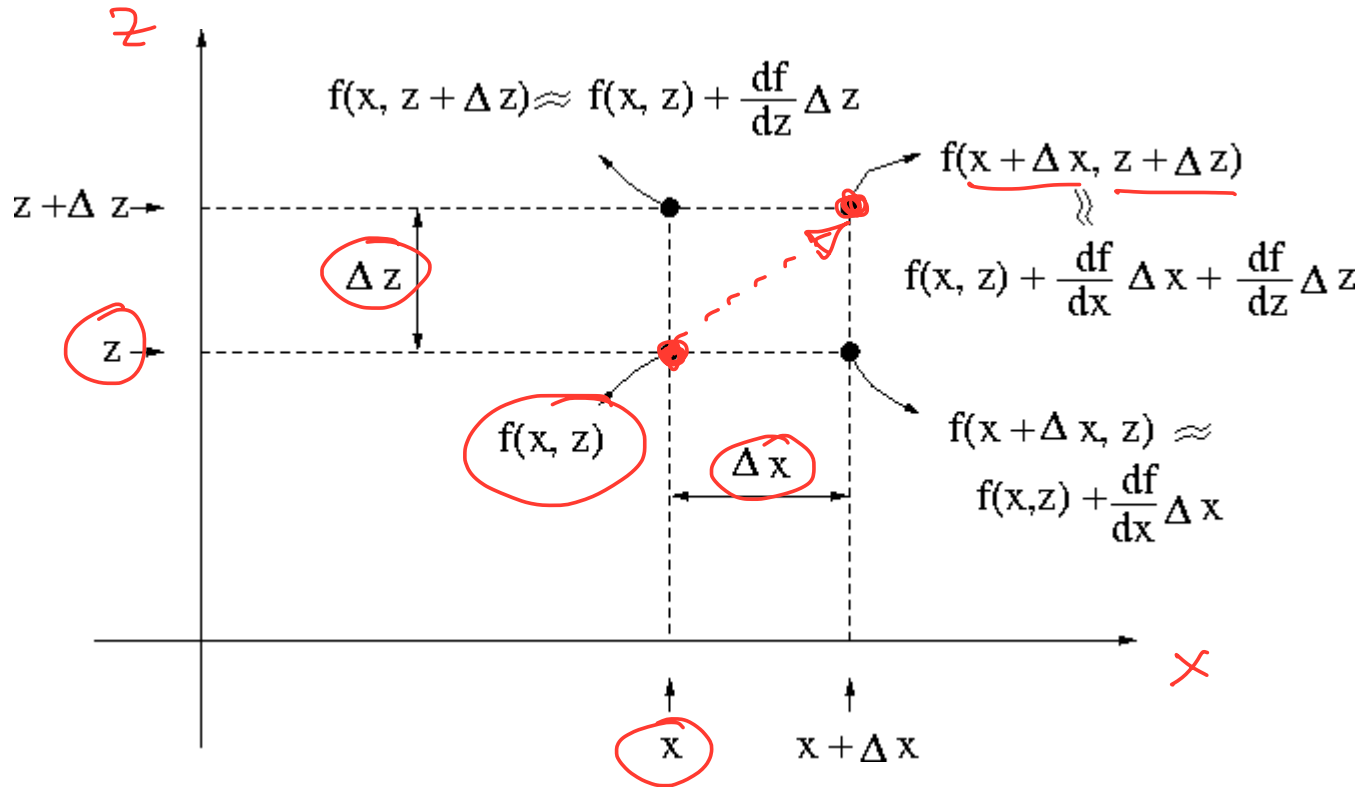
Based on Taylor expansion it can be shown

$$e^x \approx 1 + x$$

$$\tan \theta \approx \theta$$

θ in RADIANS

1st ORDER APPROXIMATION IN 2-D



f can be any
function
 of x, z
 e.g. pressure,
 velocity
 of fluid,
 etc.

$$f(x + \Delta x, z + \Delta z) \approx f(x, z) + \frac{\partial f}{\partial x} \Delta x + \frac{\partial f}{\partial z} \Delta z \quad + \text{HOT} \quad (19)$$

those partial derivatives
 must be evaluated at
 the location (x, z)

EXAMPLE ON 1st ORDER APPROXIMATION IN 2-D

$$f(x, z) = x^3 + xz^2$$

$$\left. \begin{array}{l} x=1 \\ z=1 \end{array} \right\} f = 1^3 + 1 \cdot 1^2 = 2 = f(1, 1)$$

$$f\left(\underset{\substack{\downarrow \\ 1+0.1}}{1.1}, \underset{\substack{\downarrow \\ 1+0.1}}{1.1}\right) = f(1, 1) + \frac{\partial f}{\partial x} \underset{\substack{\parallel \\ 0.1}}{\Delta x} + \frac{\partial f}{\partial z} \underset{\substack{\parallel \\ 0.1}}{\Delta z}$$

$$\frac{\partial f}{\partial x} = 3x^2 + z^2 \quad \rightsquigarrow \quad \frac{\partial f}{\partial x} \Big|_{1,1} = 3 \cdot 1^2 + 1^2 = 4$$

$$\frac{\partial f}{\partial z} = 2xz \quad \rightsquigarrow \quad \frac{\partial f}{\partial z} \Big|_{1,1} = 2 \cdot 1 \cdot 1 = 2$$

$$f(1.1, 1.1) = 2 + 4 \cdot \Delta x + 2 \Delta z =$$

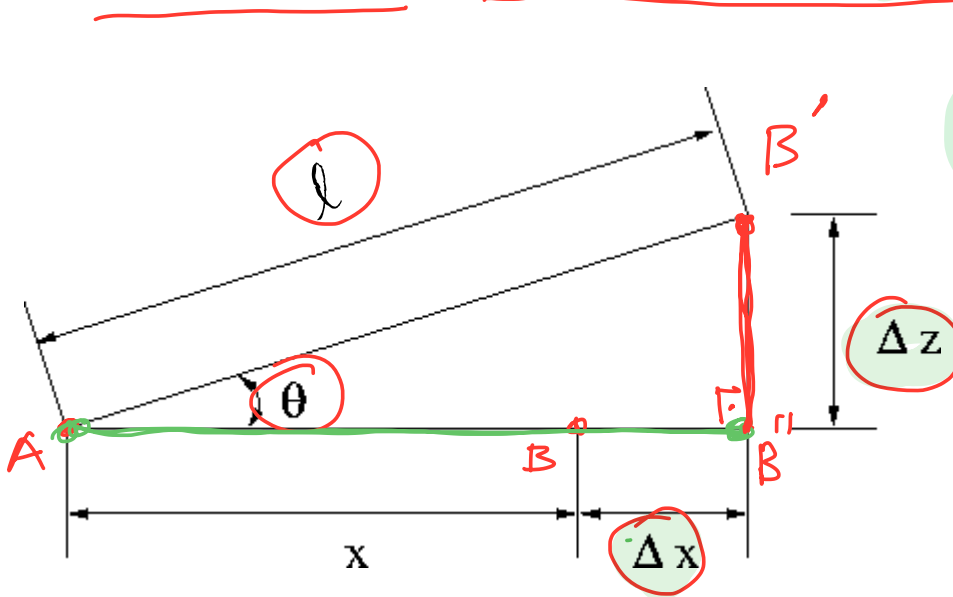
$$= 2 + 4 * (0.1) + 2 * (0.1) = \boxed{2.6} \leftarrow \text{APPROX.}$$

$$f(1.1, 1.1) = \boxed{2.662} \text{ (exact)}$$

$$\% \text{ error} = -2.3\%$$

SOME USEFUL APPROXIMATIONS

Q: How can l and θ be approximated for "small" values of $\Delta x, \Delta z$ compared to x ?



$$l \approx 1 + \Delta x = \underline{\underline{AB''}}$$

$$\tan \theta \approx \theta$$

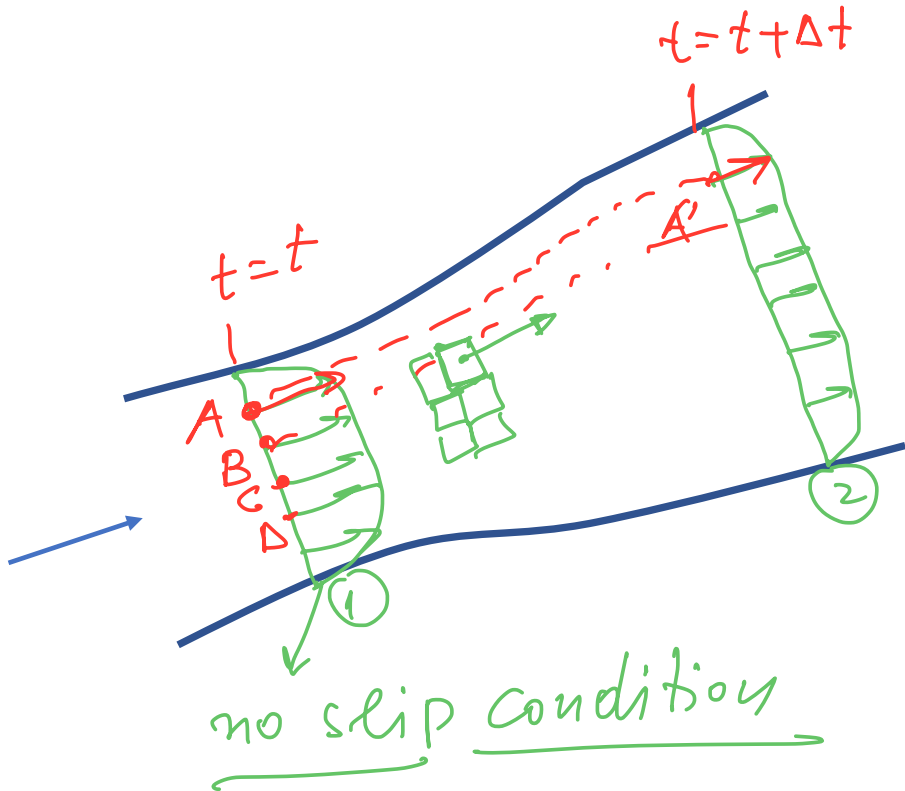
θ in RADIANS

$$= \frac{\Delta z}{x + \Delta x} =$$

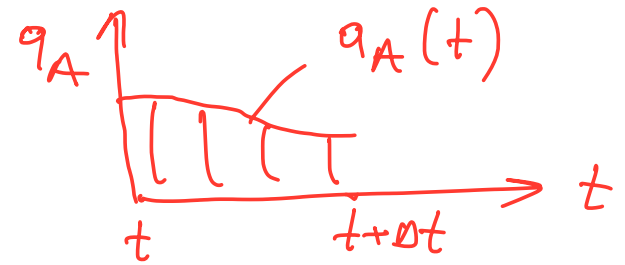
$$= \frac{\Delta z}{x \left(1 + \frac{\Delta x}{x}\right)} = \frac{\Delta z}{x} \frac{1}{\left(1 + \frac{\Delta x}{x}\right)} \approx$$

$$\frac{\Delta z}{x} \left[1 - \frac{\Delta x}{x}\right] = \frac{\Delta z}{x} - \frac{\Delta z \Delta x}{x^2} \text{HOT} = \frac{\Delta z}{x}$$

TWO APPROACHES TO DEFINE A FLOW-FIELD



LAGRANGIAN APPROACH

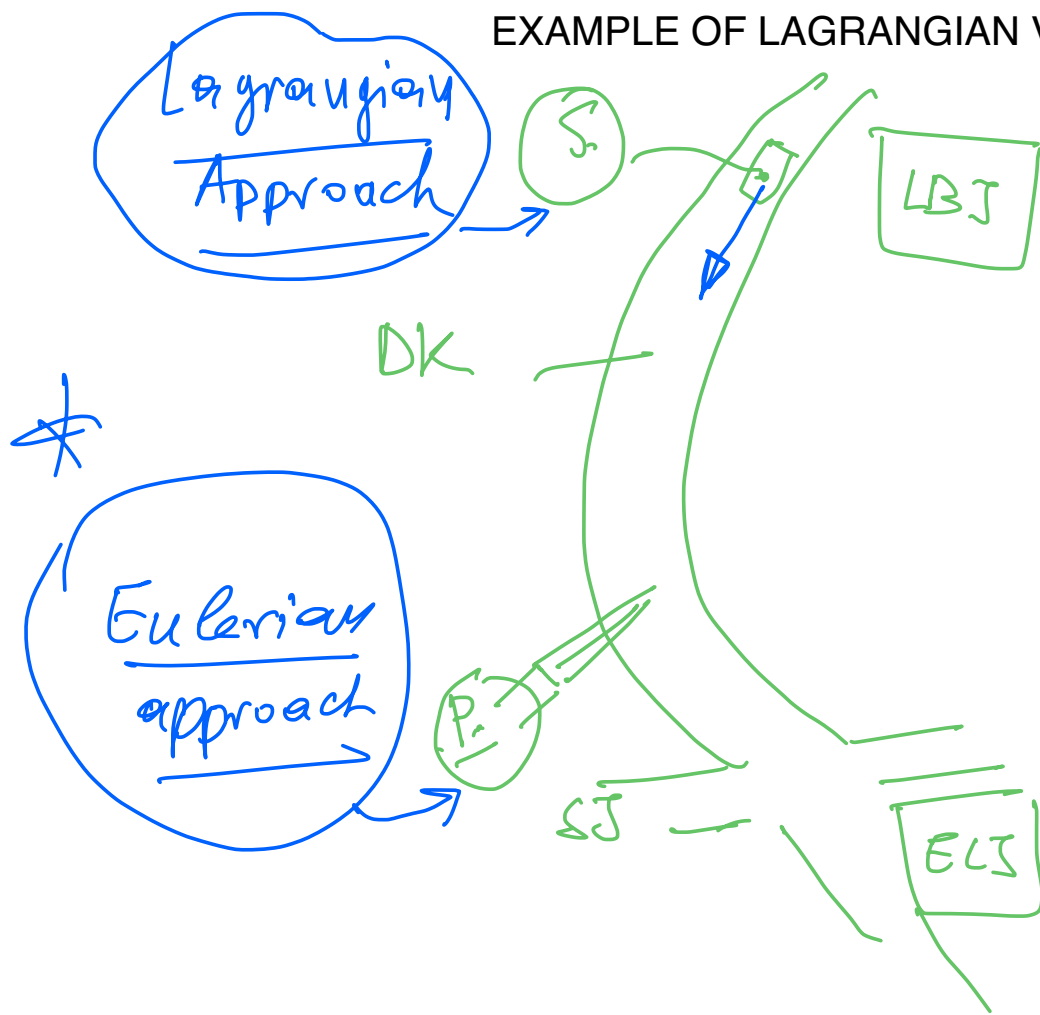


Follows the particle and records its velocity

EULERIAN APPROACH

It does not follow the particles.
Record velocities of particles that pass through a fixed point.

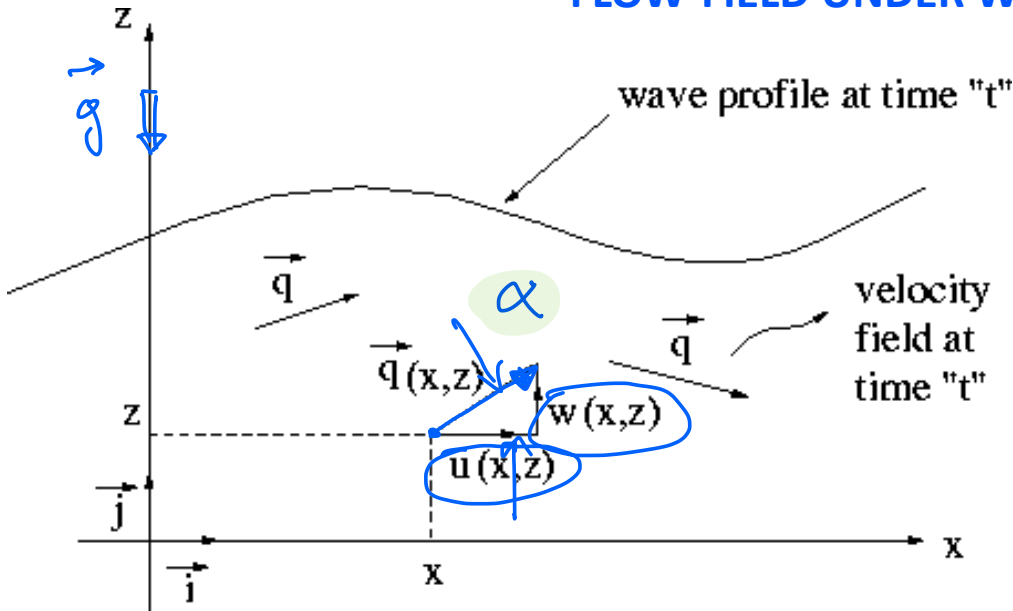
EXAMPLE OF LAGRANGIAN VS. EULERIAN APPROACH



S: Spyros in his car, checks his speed on the speedometer

P: Police measure speeds of cars passing through fixed location

FLOW-FIELD UNDER WAVE SURFACE



Q: What laws should the fluid field follow?

$\begin{bmatrix} u(x, z) \\ w(x, z) \end{bmatrix}$ components of velocity vector \vec{q}

Laws of Physics!

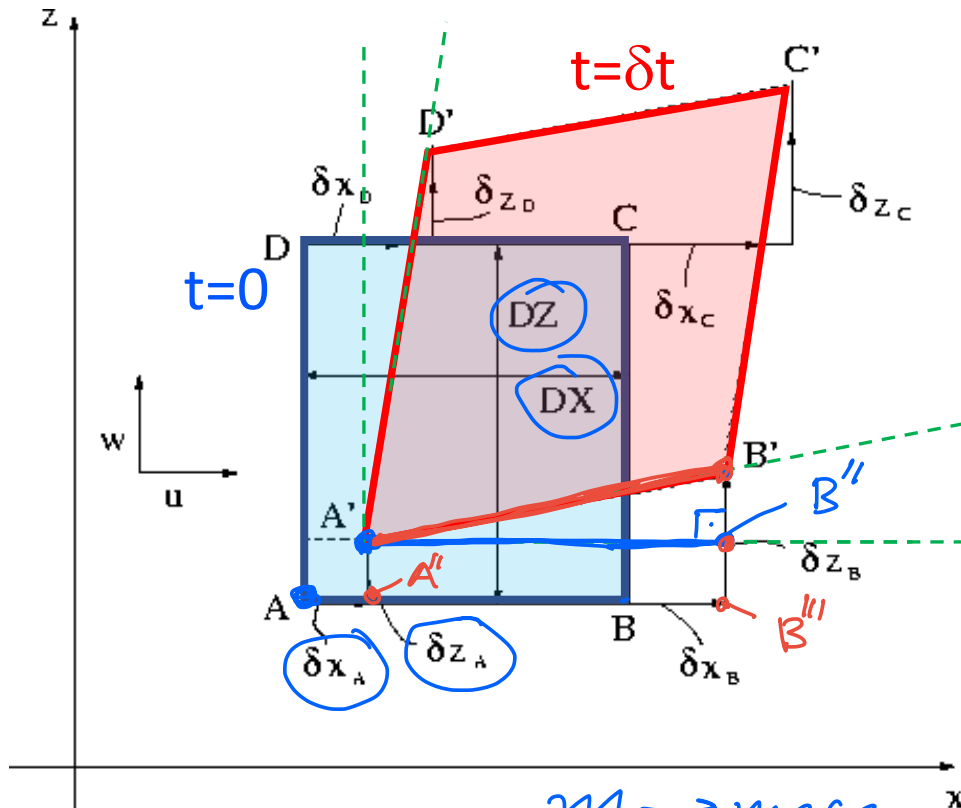
$$q = |\vec{q}| = \sqrt{u^2 + w^2}$$

$$\tan \alpha = \frac{w}{u}$$

angle α of velocity vector with horizontal axis x

magnitude of velocity vector

DEFORMATION OF FLUID PARTICLE & CONSERVATION OF MASS



$$m_{ABCD} = m_{A'B'C'D'}$$

$$\rho \nabla_{ABCD} = \rho' \nabla_{A'B'C'D'}$$

Incompressible flow

$$\rho = \rho'$$

$$\nabla_{ABCD} = \nabla_{A'B'C'D'}$$

$$DX \cdot DZ = (A'B'C'D')$$

If u_A, w_A are the velocities at A

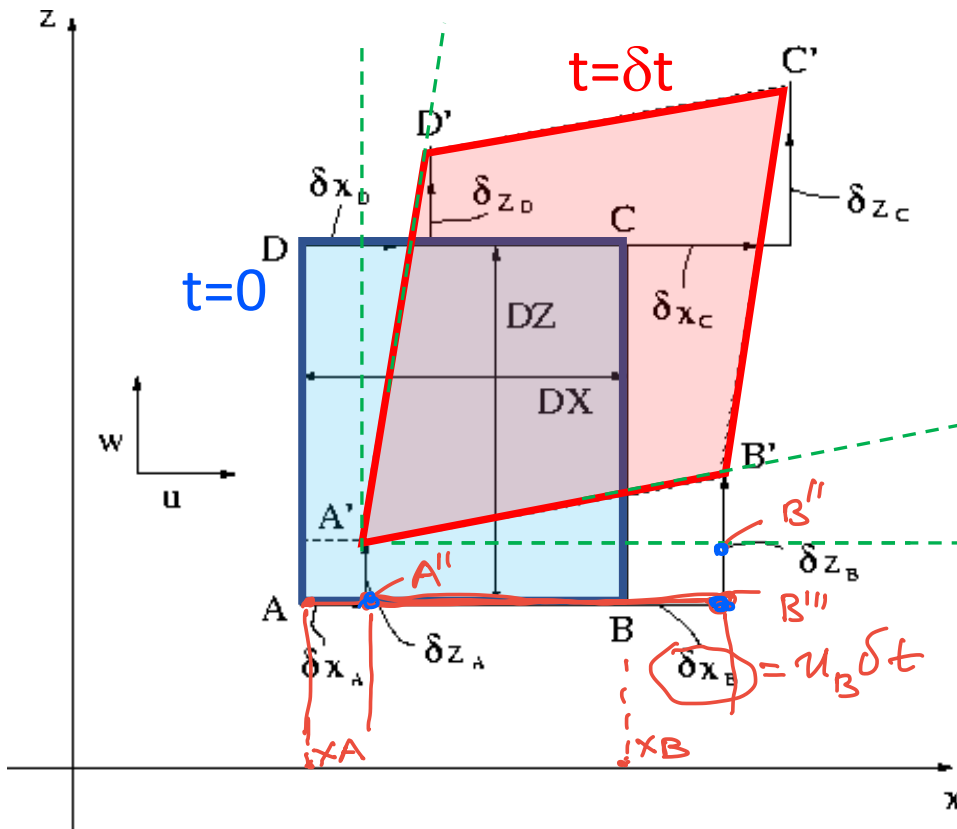
$$\text{then } \begin{cases} \delta x_A = u_A \delta t \\ \delta z_A = w_A \delta t \end{cases}$$

density $\rightarrow \rho = \frac{m \rightarrow \text{mass}}{\nabla \rightarrow \text{volume}}$

$$(A'B'C'D') \approx (A'B')(A'D')$$

$(A'B'')$
 $C = A''B'''$

DEFORMATION OF FLUID PARTICLE & CONSERVATION OF MASS



$$A''B''' = AB''' - AA'' = (AB + BB''')$$

$$\begin{aligned} \rightarrow AB + BB'' - AA'' &= \\ &= DX + u_B \delta t - u_A \delta t = \\ &= DX + (u_B - u_A) \delta t \end{aligned}$$

Taylor in 2-D: $u(x_B, z_B) = u(x_A, z_A) + \frac{\partial u}{\partial x} \Delta x + \frac{\partial u}{\partial z} \Delta z$

$(z_B = z_A)$

$$\rightarrow u_B = u_A + \frac{\partial u}{\partial x} DX$$

$$\rightarrow (u_B - u_A) = \frac{\partial u}{\partial x} DX$$

$$\begin{aligned} A'B'' &= A'B''' = \\ &= DX + \frac{\partial u}{\partial x} DX \delta t \\ &= DX \left[1 + \frac{\partial u}{\partial x} \delta t \right] \end{aligned}$$

CONTINUITY EQUATION FOR INCOMPRESSIBLE FLUIDS

$$A'B' = D_x \left[1 + \frac{\partial u}{\partial x} \delta t \right]$$

Similarly: $A'D' = D_z \left[1 + \frac{\partial w}{\partial z} \delta t \right]$

Due to conservation of mass \rightarrow

$$(A'B'C'D') = (A'B')(A'D') = D_x D_z \left[1 + \frac{\partial u}{\partial x} \delta t \right] \left[1 + \frac{\partial w}{\partial z} \delta t \right]$$

$$= (ABCD) = D_x D_z$$

$$\cancel{D_x D_z} = \cancel{D_x D_z} \left[1 + \frac{\partial u}{\partial x} \delta t + \frac{\partial w}{\partial z} \delta t + \frac{\partial u}{\partial x} \frac{\partial w}{\partial z} (\delta t)^2 \right]$$

$$\cancel{1} = \cancel{1} + \frac{\partial u}{\partial x} \delta t + \frac{\partial w}{\partial z} \delta t + \frac{\partial u}{\partial x} \frac{\partial w}{\partial z} (\delta t)^2$$

HOT \nearrow

$$\left(\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right) \delta t = 0$$

$$\Rightarrow \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

Continuity equation

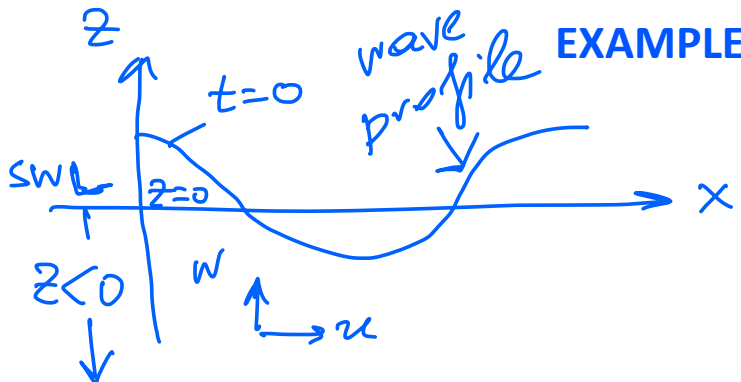
must be valid at ALL points and at ALL times

Valid for steady and unsteady flow

Valid for inviscid or viscous flow

In 3-D:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$



EXAMPLE ON CONTINUITY EQUATION

Flow field under the wave can be expressed as follows:

(we will prove that later)

- $u = e^{\lambda z} \cos(kx) k$
 - $w = \lambda e^{\lambda z} \sin(kx)$
- $\lambda = ?$

$\frac{de^x}{dx} = e^x$

$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$

$\frac{\partial u}{\partial x} = e^{\lambda z} [-\sin(kx) k] k = -e^{\lambda z} k^2 \sin(kx)$

$\frac{\partial w}{\partial z} = \lambda e^{\lambda z} \lambda \sin(kx) = e^{\lambda z} \lambda^2 \sin(kx)$

$-e^{\lambda z} k^2 \sin(kx) + e^{\lambda z} \lambda^2 \sin(kx) = 0$

$e^{\lambda z} \sin(kx) [-k^2 + \lambda^2] = 0$

must be valid for ALL x, z

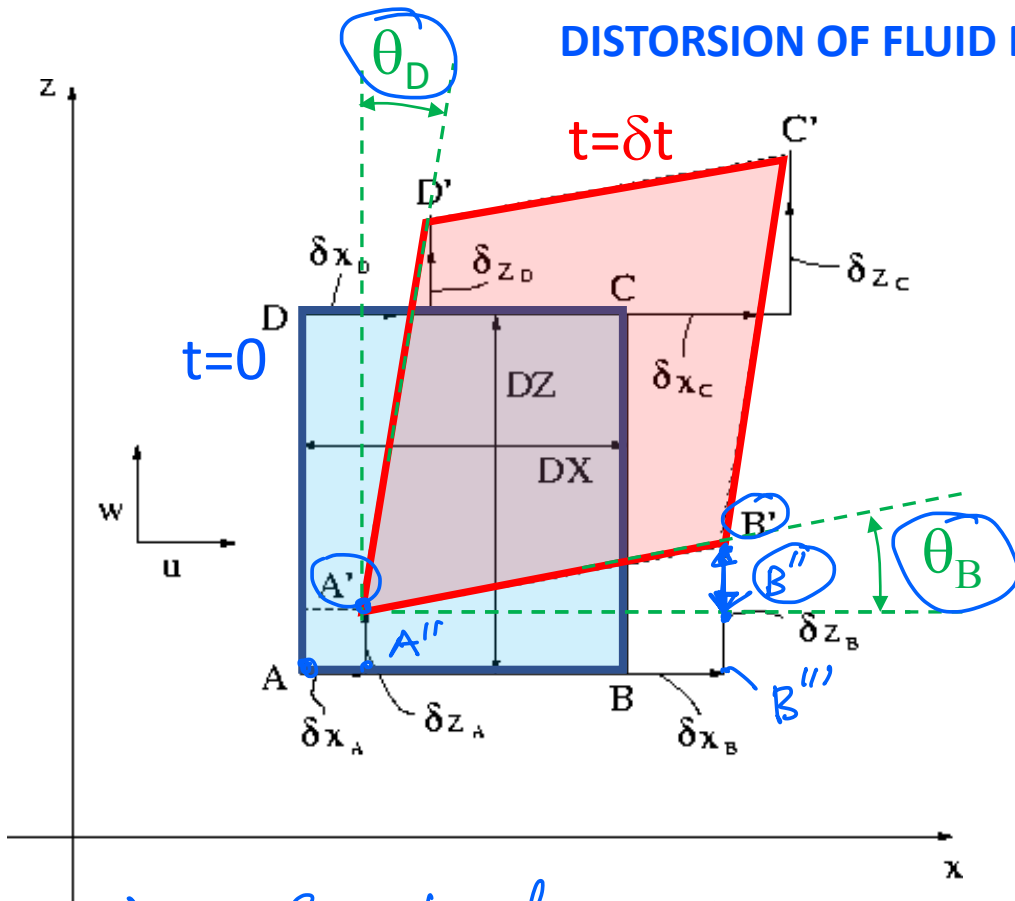
$-k^2 + \lambda^2 = 0 \rightsquigarrow \lambda = \pm k$

if $\lambda = -k$ then $e^{\lambda z} = e^{-kz}$ would blow up as $z \rightarrow -\infty$

Thus $\lambda = +k$ provides a physical solution

NOT Physical

DISTORSION OF FLUID PARTICLE



$$\theta_B \approx \tan \theta_B = \frac{(B'B'')}{(A'B'')}$$

$$B'B'' = B'B''' - B''B'''$$

$\underbrace{\hspace{1.5cm}}_{W_B \Delta t} \quad \underbrace{\hspace{1.5cm}}_{W_A \Delta t}$

$$\Rightarrow = (W_B - W_A) \Delta t =$$

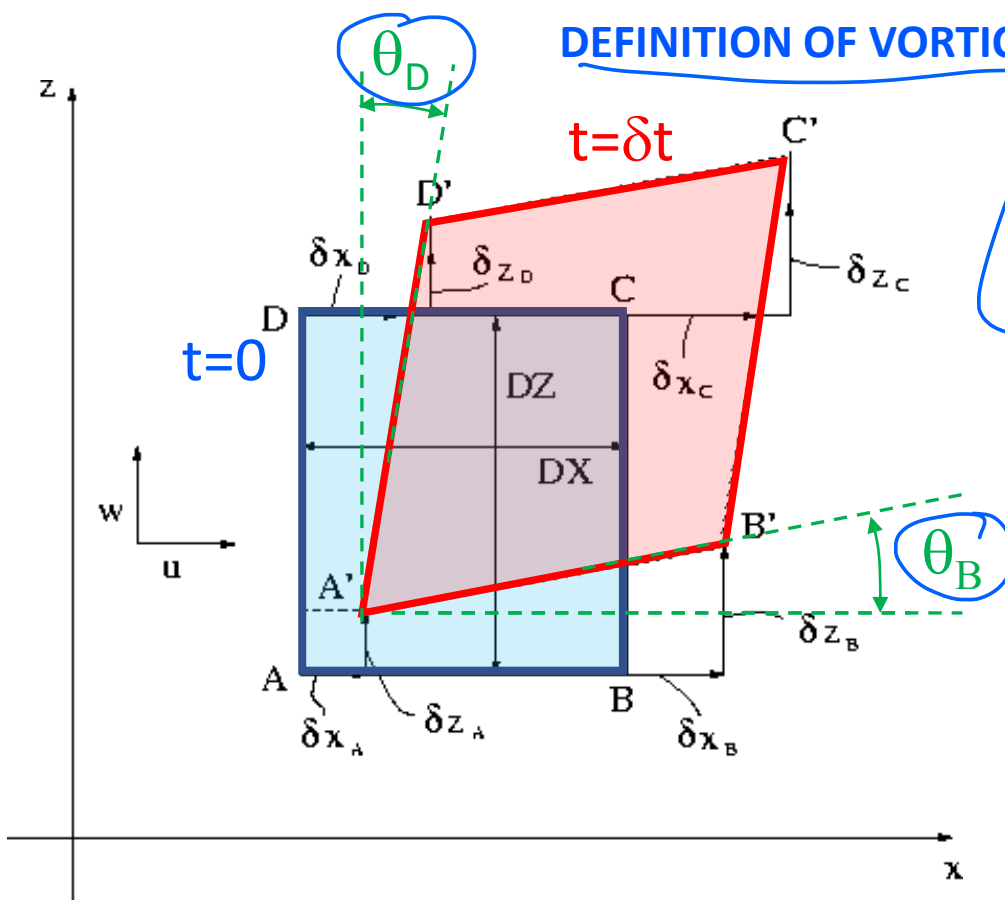
$$= \frac{\partial W}{\partial X} DX \Delta t$$

We already have from above: $A'B'' = DX \left[1 + \frac{\partial u}{\partial x} \Delta t \right]$

$$A_B = \frac{\frac{\partial w}{\partial x} DX \Delta t}{DX \left[1 + \frac{\partial u}{\partial x} \Delta t \right]} = \frac{\frac{\partial w}{\partial x} \Delta t}{\left[1 + \frac{\partial u}{\partial x} \Delta t \right]} = \frac{\partial w}{\partial x} \Delta t \left[1 - \frac{\partial u}{\partial x} \Delta t \right] =$$

We used binomial approx
 $\frac{1}{1+\alpha} = 1-\alpha$

$$= \frac{\partial w}{\partial x} \Delta t - \frac{\partial w}{\partial x} \frac{\partial u}{\partial x} \Delta t^2 \quad \text{HOT} = \boxed{\left(\frac{\partial w}{\partial x} \right) \Delta t}$$



DEFINITION OF VORTICITY

$$\vartheta_D = \left(\frac{\partial u}{\partial z} \right) \delta t$$

similarly we get

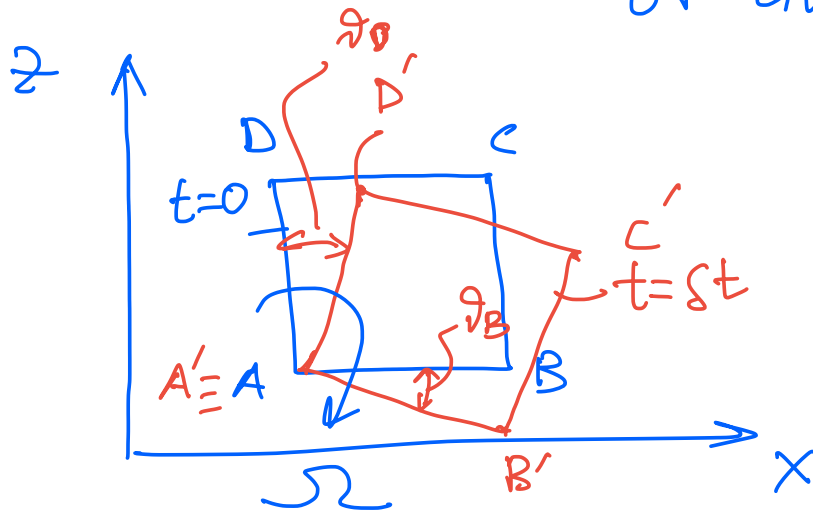
$$\omega = \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x}$$

$$\omega = \frac{\vartheta_D}{\delta t} - \frac{\vartheta_B}{\delta t} = \frac{\vartheta_D - \vartheta_B}{\delta t}$$

mathematical definition of vorticity, ω

PHYSICAL MEANING OF VORTICITY

Special case: Particle subject to "Spin" or angular speed Ω



$$\omega = \frac{v_D - v_B}{\delta t}$$

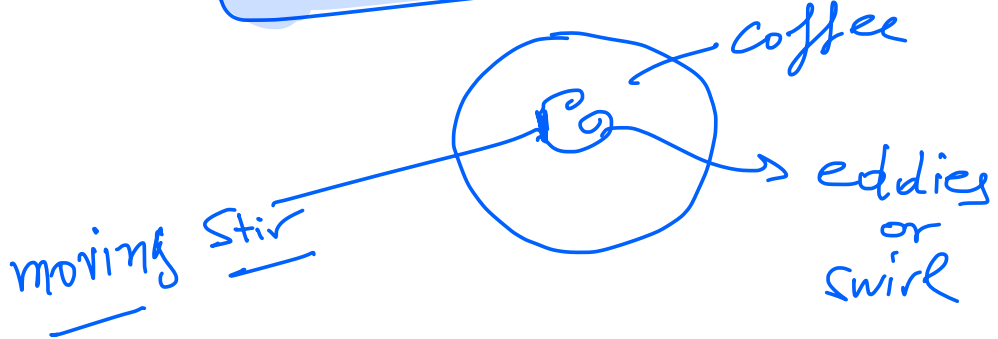
$$v_D = \Omega \delta t$$

$$v_B = -\Omega \delta t$$

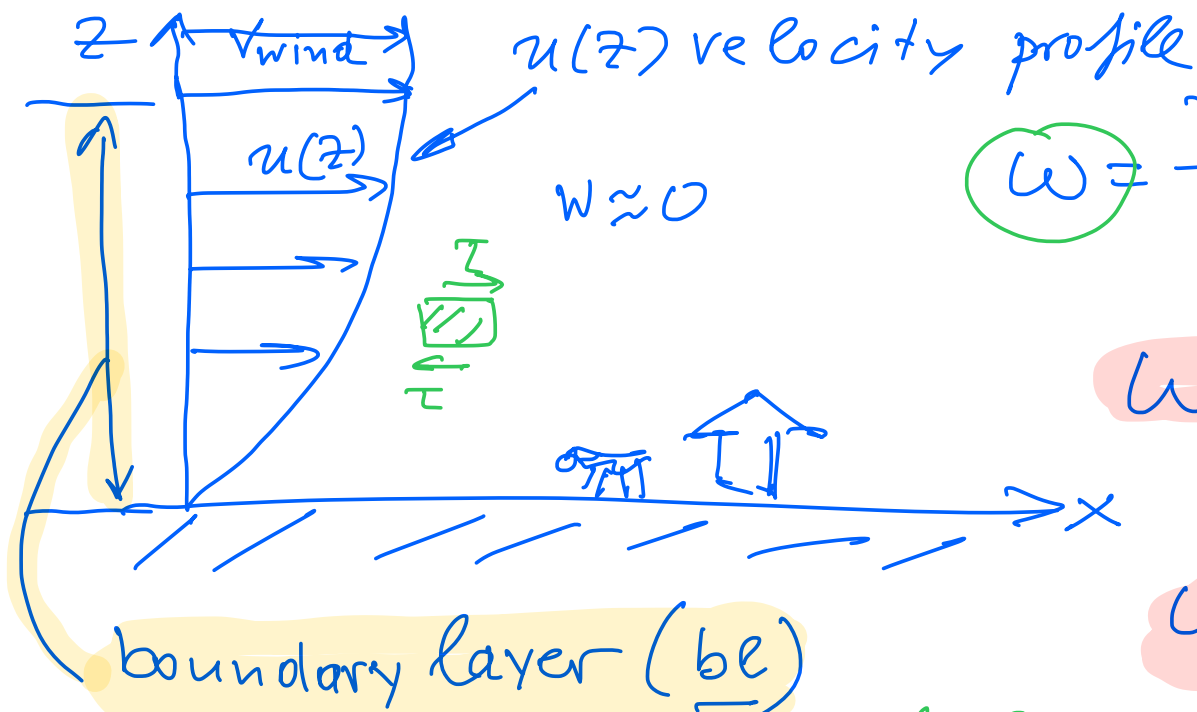
$$\Rightarrow \omega = \frac{\Omega \delta t - (-\Omega \delta t)}{\delta t}$$

$$\omega = 2\Omega$$

Vorticity is directly related to spin of particle



} other "words" for vorticity



$$\omega = \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} = \frac{\partial u}{\partial z}$$

= 0

$\omega = 0$ outside the be

$\omega \neq 0$ inside the be

ω_{max} at the ground

ω is proportional to τ

ω is significant where τ is significant

τ : shear stress of fluid particles

$$\tau = \mu \frac{\partial u}{\partial z} \rightarrow \tau = \mu \cdot \omega$$

dynamic (or absolute) viscosity

DEFINITION OF IRROTATIONAL FLOW

