

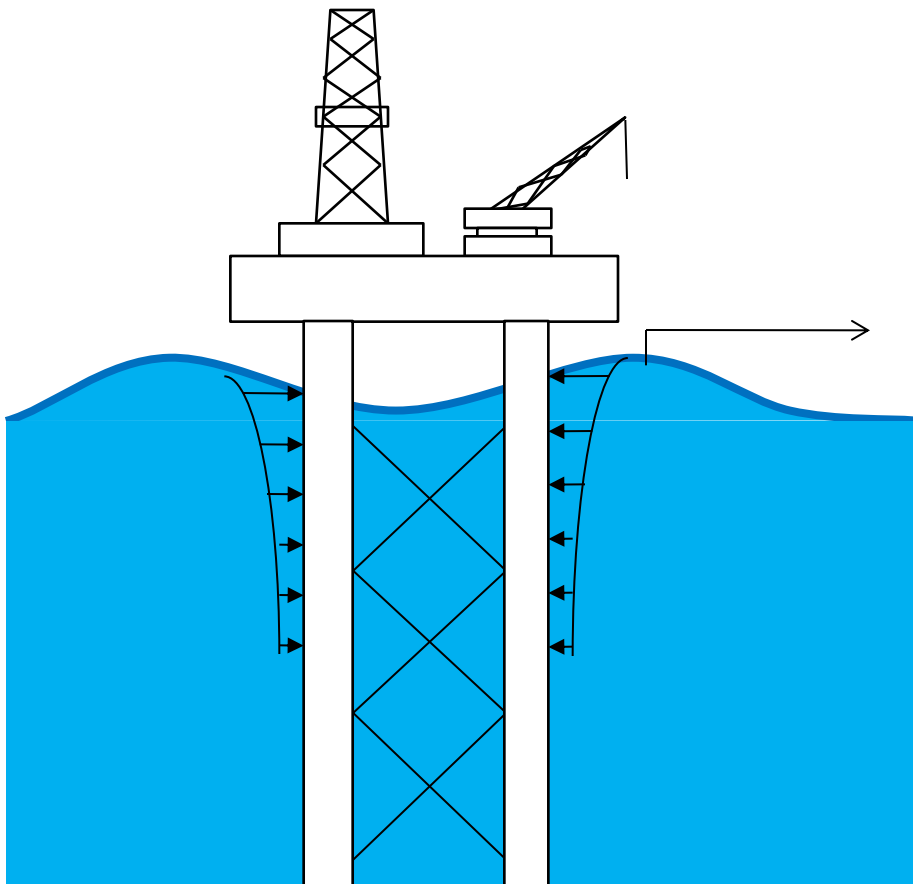
2013 Short Course on Fundamentals of Offshore Structures and Design of Fixed Offshore Platforms

April 15-26, 2013, UT Austin

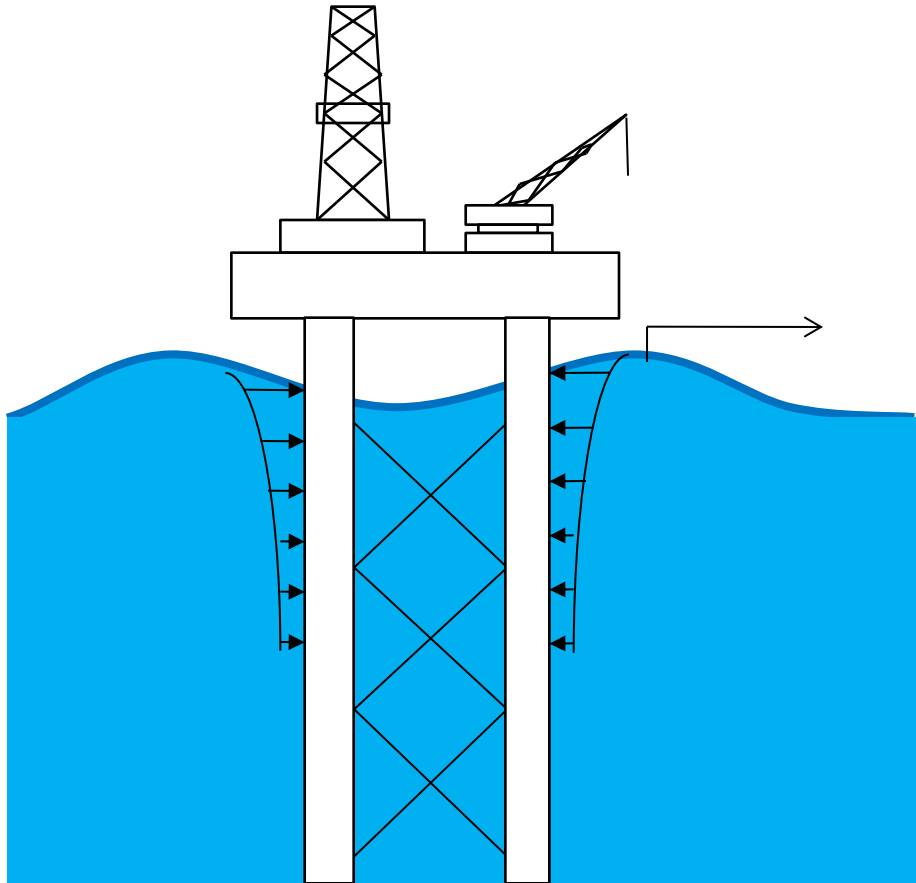
Wave Theory and Applications

by

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To determine wave forces on an offshore structure we need to know *fluid velocities & accelerations* under the wave surface



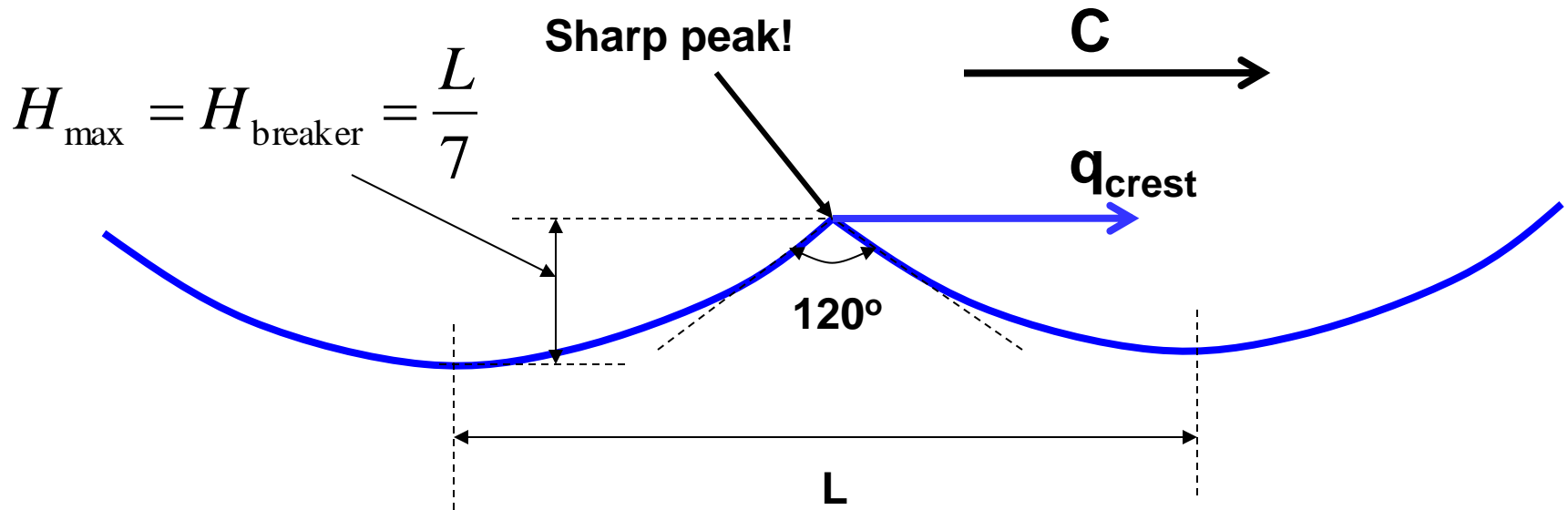
An offshore structure is designed to withstand the 100-year storm (wave/current/wind). A **mono-chromatic wave of height H_{\max}** is assumed.

H_{\max}/L is larger than required for linear wave theory to be valid.

*Wave velocities and accelerations from linear wave theory, when used in Morison's equation, **under-predict** wave forces!*

What is the maximum height a wave in deep water can have (before it breaks)?

Stokes' Criterion for wave breaking: $q_{\text{crest}}=C$



Q: How well could linear theory handle waves at breaking?
A: Pretty BAD! (predicts $H_{\text{max}}=L/\pi$ in deep water!)

Stokes' 2nd order non-linear wave theory (1/2)

$$\eta(x,t) = \frac{H_1}{2} \cos(kx - \omega t) + \frac{H_2}{2} \cos[2(kx - \omega t)]$$

1st order term

2nd order term

$$H_1 = H \quad \text{and} \quad H_2 = \frac{\pi H^2}{4 L} \frac{\cosh(2\pi d / L)}{\sinh^3(2\pi d / L)} [2 + \cosh(4\pi d / L)]$$

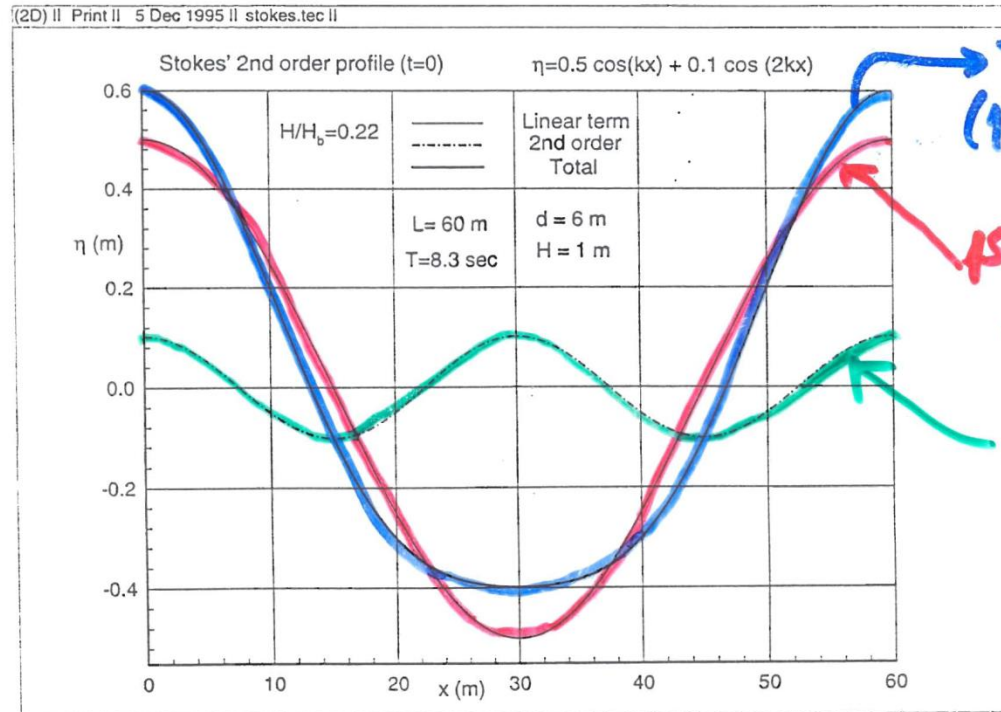
Case 1

$$d = 6 \text{ m}, H = 1 \text{ m}$$

$$L = 60 \text{ m}, T = 8.3 \text{ sec}$$

$$H / L = 1 / 60$$

$$d / L = 0.1$$



Stokes' 2nd order non-linear wave theory (2/2)

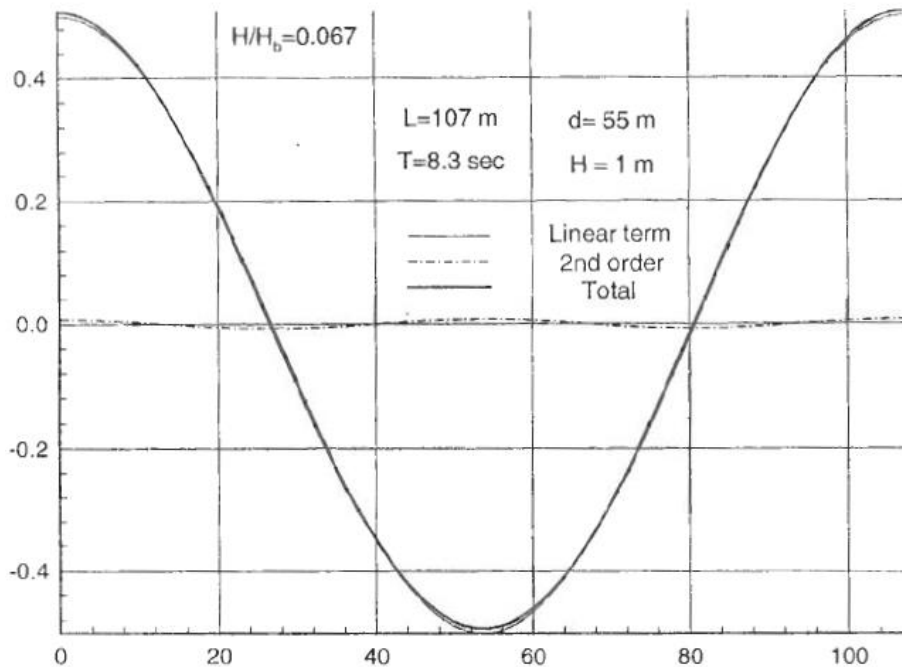
Case 2

deep water, $H = 1m$
 $T = 8.3$ (same as in Case 1)
 $L = 107m$
 $H / L = 1/107$

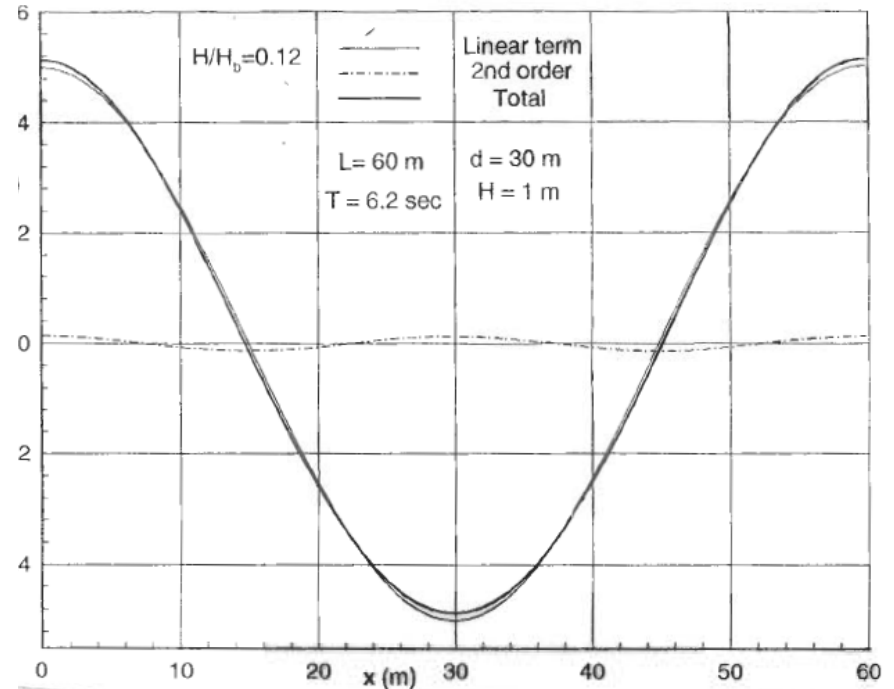
Case 3

deep water, $H = 1m$
 $L = 60m$ (same as Case 1)
 $T = 6.2$ sec
 $H / L = 1/60$

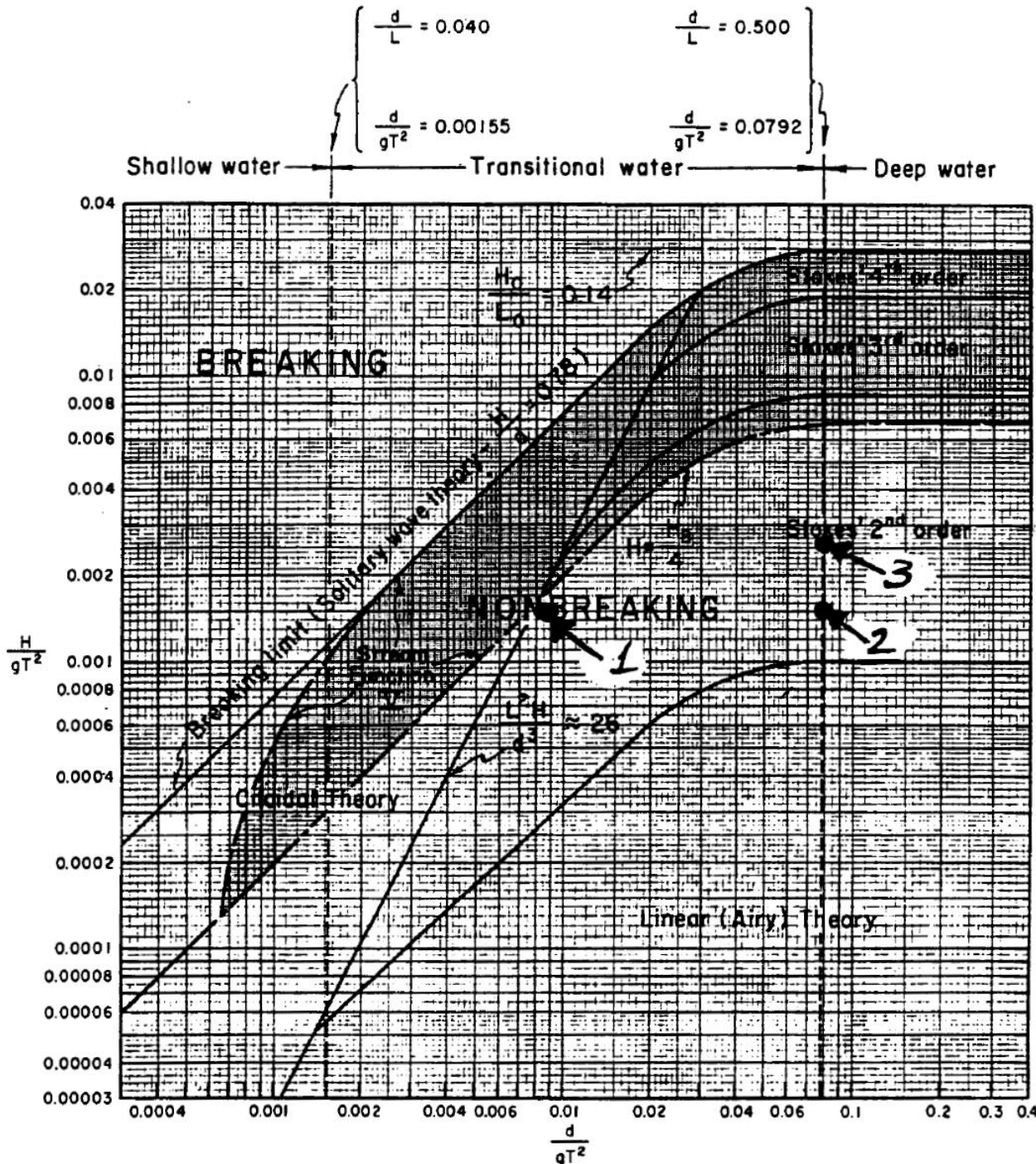
Stokes' 2nd order profile (t=0)

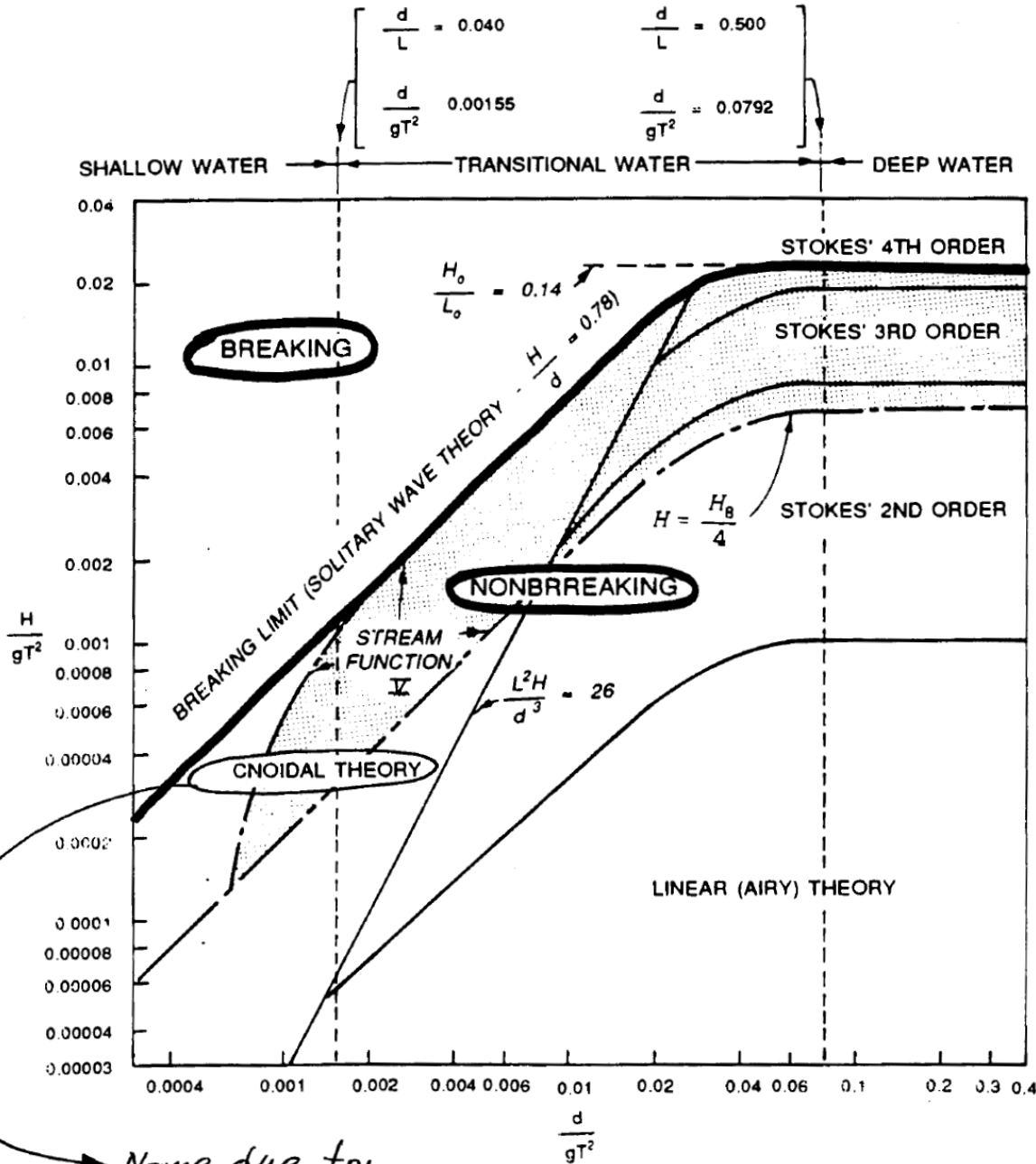


Stokes' 2nd order profile (t=0)



Cases 1, 2, & 3 on the graph by Le Mehaute



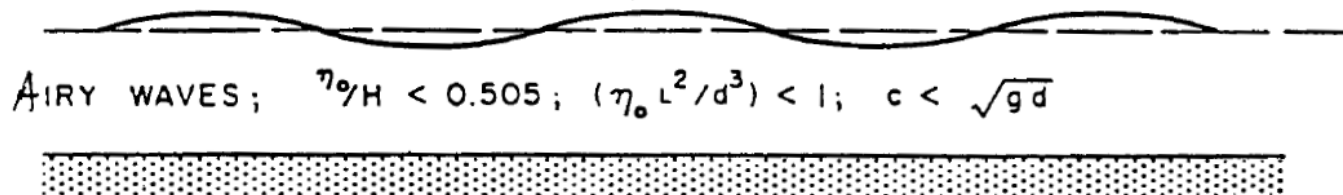
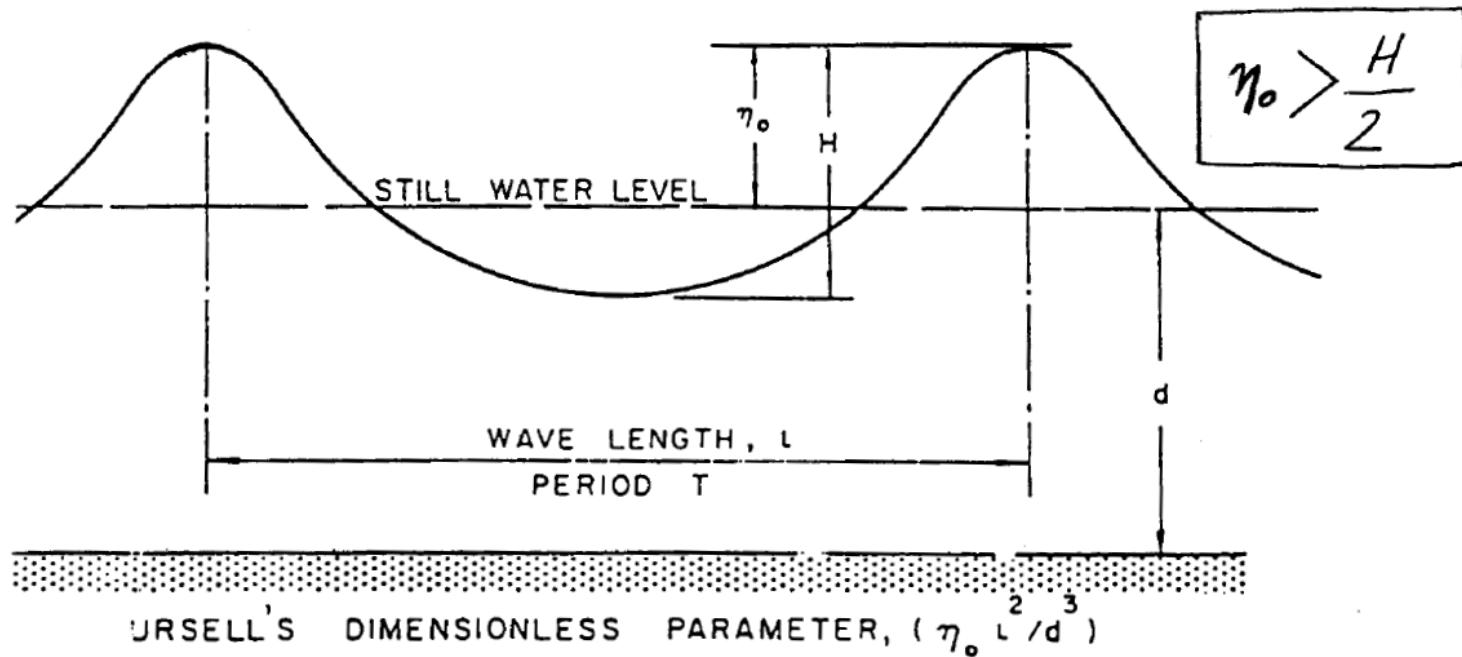


A cleaner version of the graph by Le Mehaute

Name due to:
cn: elliptic cosine function

(after Le Mehaute, 1969)

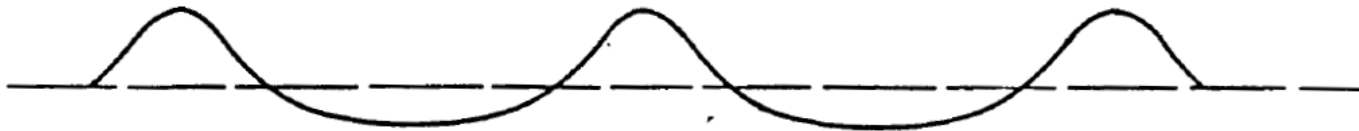
Different types of waves (1/2):



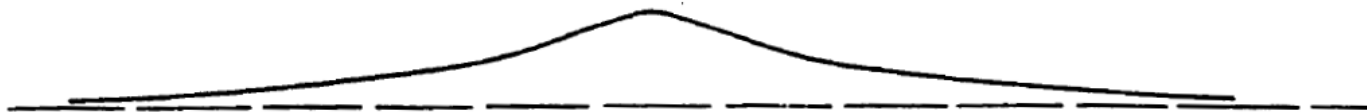
Different types of waves (2/2):



STOKES' WAVES; $\eta_0/H < 0.635$; $(\eta_0 L^2/d^3) < 30$; $c \leq \sqrt{gd}$



CNOIDAL WAVES; $0.635 < \eta_0/H < 1$; $(\eta_0 L^2/d^3) > 10$; $c \geq \sqrt{gd}$



SOLITARY WAVES; $\eta_0/H = 1$; $(\eta_0 L^2/d^3 \rightarrow \infty)$; $c = 1.33 \sqrt{gd}$

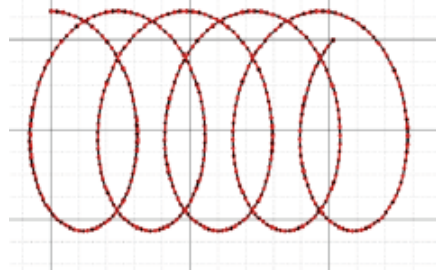


∴ 3.18. Profile shape of gravity water waves [Wilson (1963)]

Short-comings of linear wave theory:

➤ Does not produce accurate wave profiles for some combinations of d/gT^2 and H/gT^2 , and cannot handle waves just before breaking

➤ **Does not allow for mass transfer** along the wave direction. Particle trajectories are evolving tight spirals, rather than closed, as shown here:



➤ Provides inaccurate fluid velocities and accelerations which, when used in the Morison's equation (to be described later), **under-predict the forces** acting on the elements of an offshore structure

Detailed formulas for the wave profile and the corresponding flow-field for a non-linear wave are given in the provided document:

NOTES ON FIFTH-ORDER GRAVITY WAVE THEORY