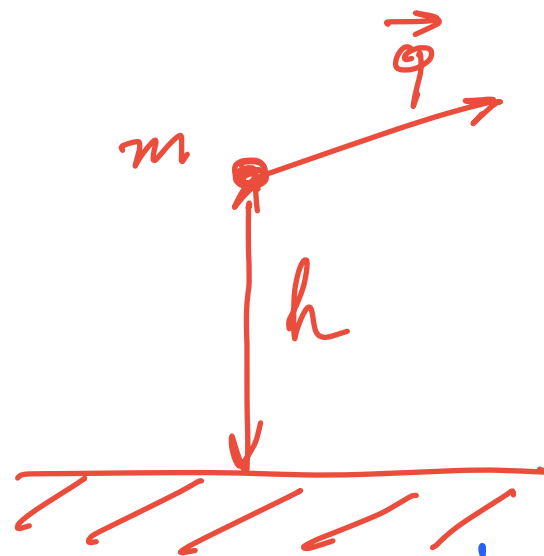


WAVE ENERGY



K.E. = Kinetic energy of m :

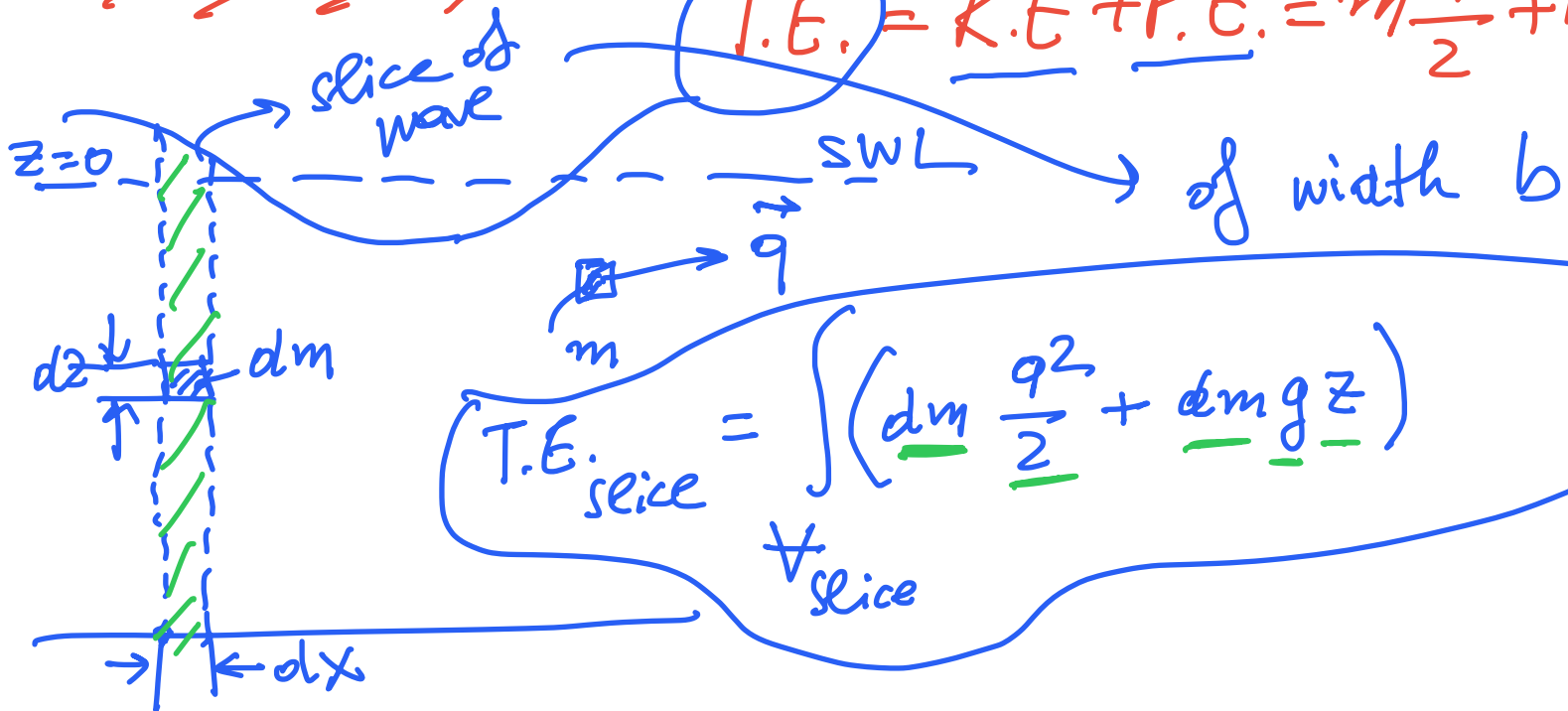
$$m \frac{q^2}{2}$$

$$q = |\vec{q}|$$

P.E. = Potential energy of m :

$$mgh$$

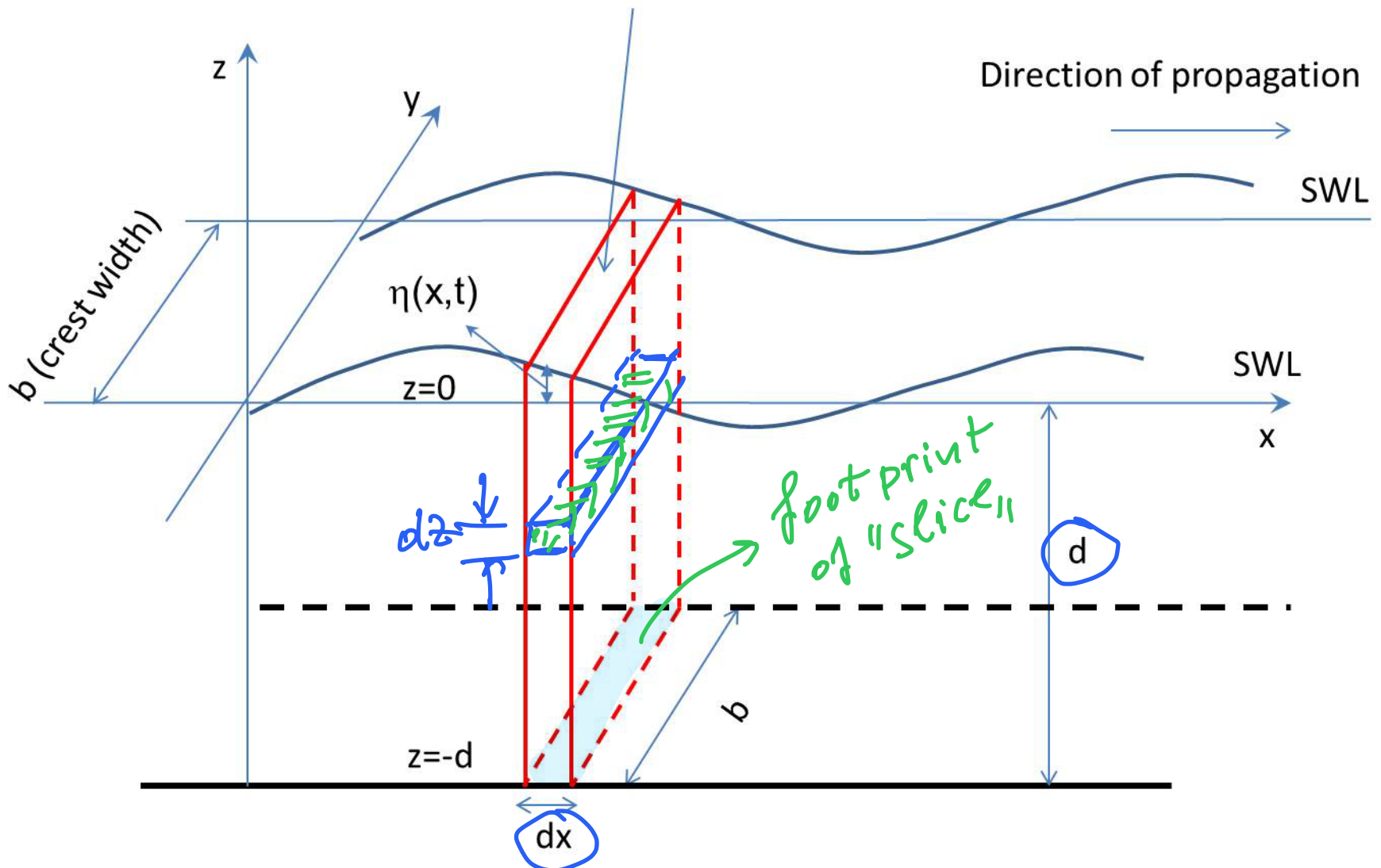
$$\text{T.E.} = \text{K.E.} + \text{P.E.} = m \frac{q^2}{2} + mgh$$



$$\text{T.E.}_{\text{slice}} = \int_{V_{\text{slice}}} \left(\underline{dm} \frac{\underline{q}^2}{2} + \underline{dm} g \underline{z} \right)$$

Perspective view of a plane progressive wave

A "Slice" of Wave Energy!



WAVE ENERGY

$$\underbrace{T.E.}_{\text{slice}} = \int_{\forall \text{ slice}} \left(\underbrace{\rho}_{\rho = \frac{dm}{dV}} \frac{q^2}{2} + \rho g z \right) dV = \underbrace{b \, dx}_{b \cdot dx} \int_{-d}^{\eta} \left(\rho \frac{q^2}{2} + \rho g z \right) dz$$

$\downarrow \bar{E}_{\text{slice}}$

$\bar{E}_{\text{slice}}$ = specific energy $\frac{T.E. \text{ slice}}{b \cdot dx}$

$b \cdot dx$ footprint of slice

$$\bar{E}_{\text{slice}} = \underbrace{\int_{-d}^{\eta} \rho \frac{q^2}{2} dz}_{\bar{E}_{\text{slice}}^k} + \underbrace{\int_{-d}^{\eta} \rho g z dz}_{\bar{E}_{\text{slice}}^p}$$

WAVE ENERGY

(Assume deep H₂O)

$$\overline{E}_{\text{slice}}^k = \int_{-d}^{\eta} \rho \frac{q^2}{2} dz = \int_{-d}^{\eta} \rho \frac{a^2 \omega^2}{2} e^{2kz} dz$$

$q = a\omega e^{kz}$

$$\rightarrow = \rho \frac{a^2 \omega^2}{2} \int_{-d}^{\eta} e^{2kz} dz = \rho \frac{a^2 \omega^2}{2} \left[\frac{e^{2kz}}{2k} \right]_{-d}^{\eta} =$$

$$= \rho \frac{a^2 \omega^2}{2} \frac{1}{2k} \left[e^{2k\eta} - e^{-2kd} \right]$$

$\xrightarrow{\text{linear theory}} e^0 = 1$
 $\cancel{e^{-2kd} = 0}$

$$\overline{E}_{\text{slice}}^k = \rho \frac{a^2 \omega^2}{4k} = \frac{\rho a^2 g}{4} = \frac{\rho H^2 g}{16} \quad a = \frac{H}{2}$$

= g dispersion relationship in deep H₂O!

$$\bar{E}_{\text{slice}}^p = \int_{-d}^{\eta} \rho g z dz = \rho g \int_{-d}^{\eta} z dz = \rho g \left. \frac{z^2}{2} \right|_{-d}^{\eta} =$$

$$= \rho g \frac{\eta^2}{2} - \rho g \frac{(-d)^2}{2} = \rho g \frac{\eta^2}{2} - \rho g \frac{d^2}{2}$$

potential
energy
associated
with waves

potential
Energy of
the standing
H₂O (without
waves)

$$\bar{E}_{\text{slice}}^p = \rho g \frac{\eta^2}{2} = \rho g \frac{a^2 \cos^2(kx - \omega t)}{2}$$

$$\eta = a \cos(kx - \omega t)$$

$$\text{From trig: } \cos^2 \theta = \frac{1 + \cos(2\theta)}{2}$$

$$\bar{E}^P_{\text{slice}} = \frac{\rho g a^2}{4} [1 + \cos(2kx - 2\omega t)]$$

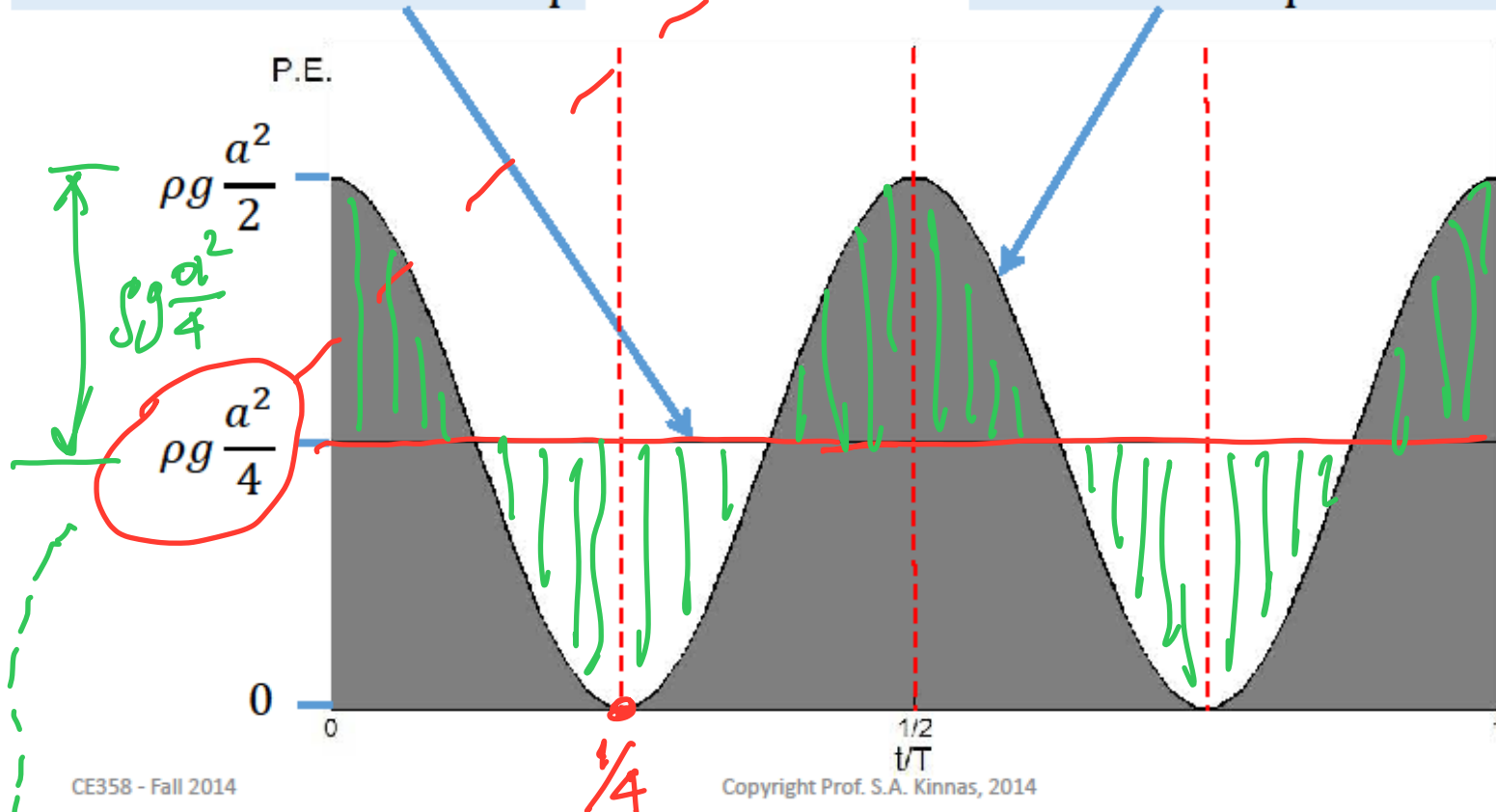
let's take $x=0$

$$\bar{E}^P_{\text{slice}} = \frac{\rho g a^2}{4} [1 + \cos(2\omega t)]$$

The potential energy (P.E.) under a sinusoidal wave

mean value of P.E. = $\rho g \frac{a^2}{4}$

P.E.(t) = $\rho g \frac{a^2}{4} \cos(2\omega t) + \rho g \frac{a^2}{4}$

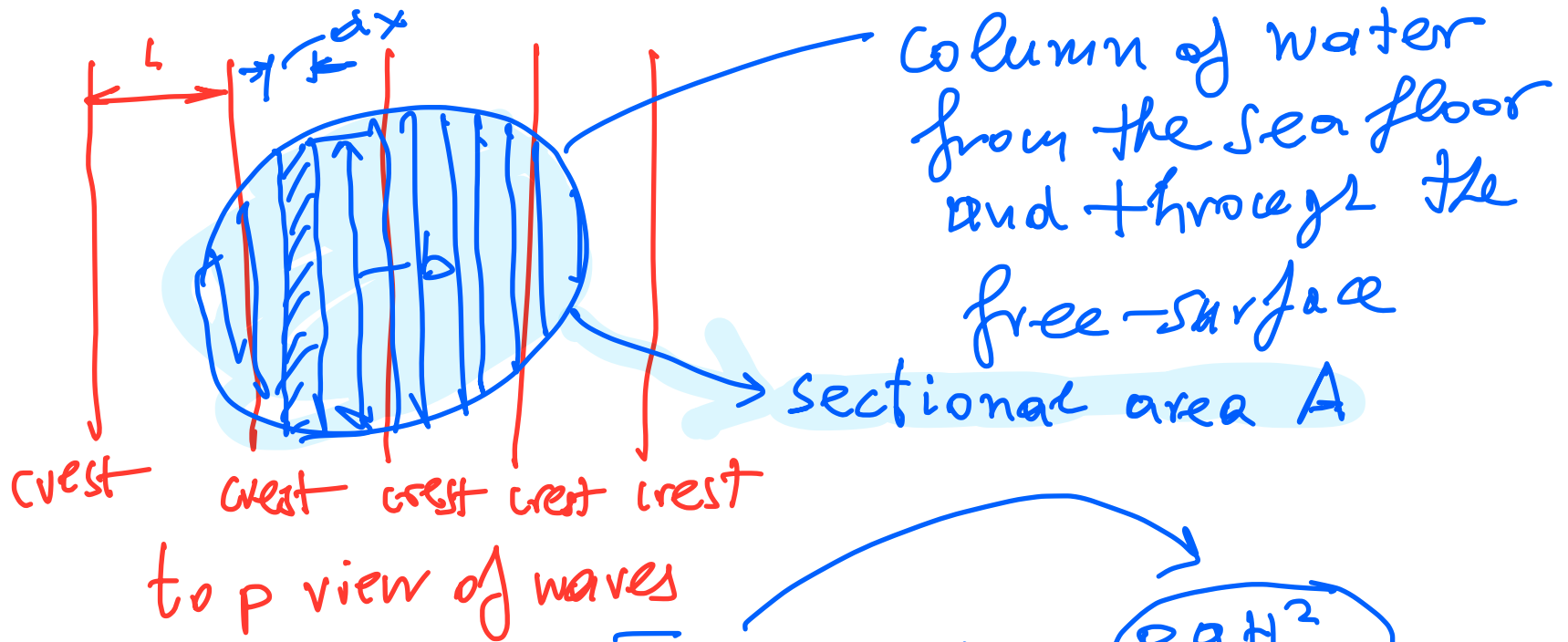


$$\omega = \frac{2\pi}{T}$$

Mean value of $\bar{E}_{slice}^p$ (over one period)
is $\frac{\rho g a^2}{4}$

$$\begin{aligned}\bar{E}_{slice} &= \bar{E}_{slice}^k + \bar{E}_{slice}^p = \\ &= 2 \bar{E}_{slice}^k = 2 \bar{E}_{slice}^p = \frac{\rho g a^2}{2}\end{aligned}$$

$\rightarrow \frac{\rho g H^2}{8} \quad (a = \frac{H}{2})$



$$E_{\text{slice}} = b dx \bar{E}_{\text{slice}} = \underline{b dx} \left(\frac{\rho g H^2}{8} \right)$$

$$\sum_{\text{All slices}} E_{\text{slice}} = \frac{\rho g H^2}{8} \int b dx$$

All slices

$A = \int b dx$ = sectional area of the column of water

(in Joules in SI)

$$E_{\text{column}} = A \frac{\rho g H^2}{8}$$

$$\bar{E}$$

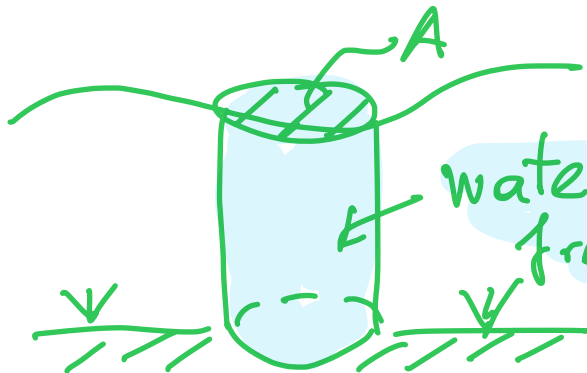
specific energy
or
energy density

$$\frac{\rho g H^2}{2}$$

Energy per unit sectional area
of water column

$$E_{\text{column}} = \bar{E} A$$

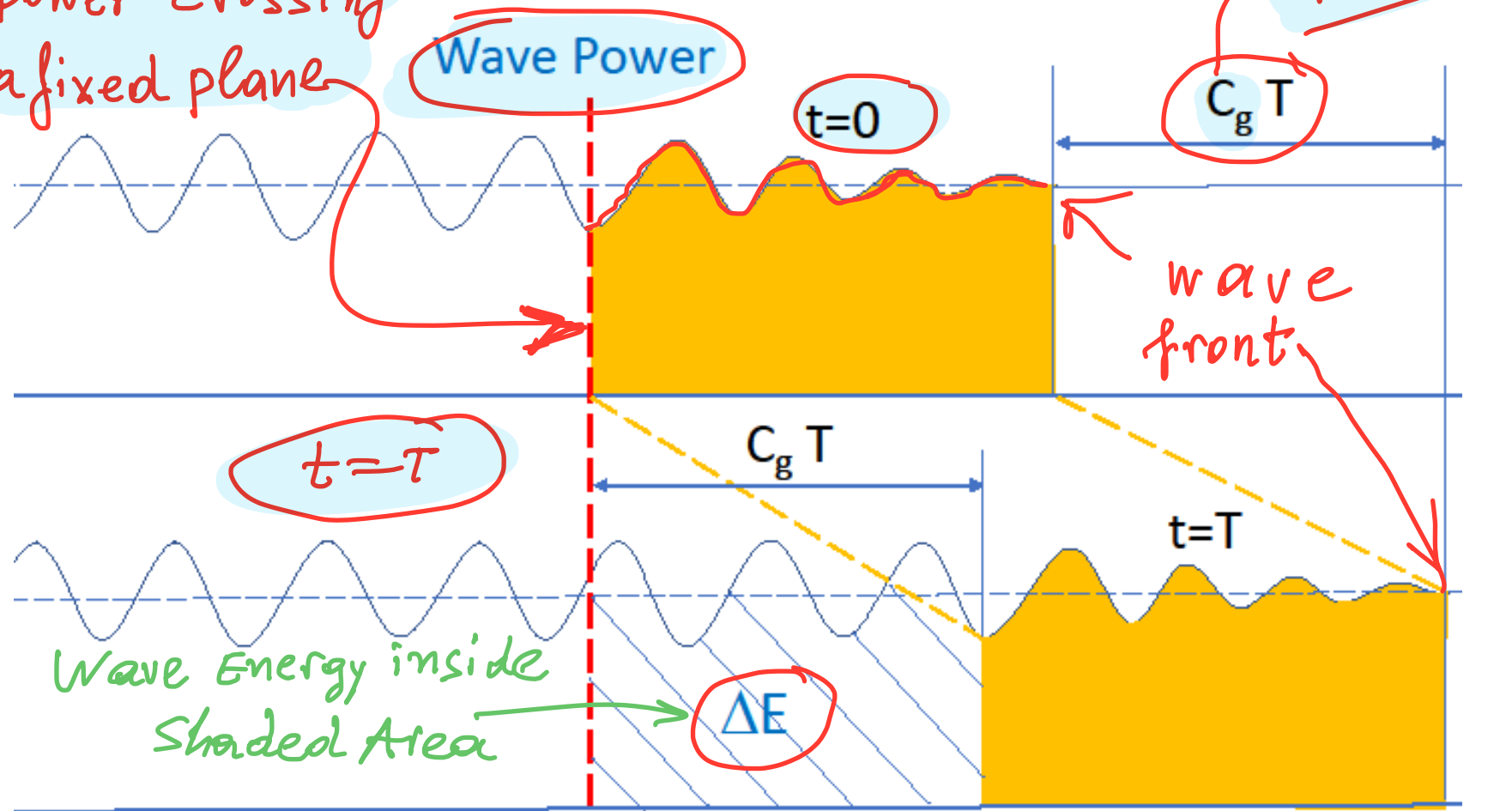
VALID FOR DEEP, TRANSI-
TIONAL & SHALLOW WATER!



water column extending
from sea-floor through
free surface

Defined as wave power crossing a fixed plane

WAVE POWER



We consider a width b

Power; $P = \Delta E / T = \bar{E} C_g T b / T = \bar{E} C_g b$

distance perpendicular to screen

WAVE POWER

$$\boxed{P} = \boxed{\text{Power}} \text{ (of the wave)} = \bar{E} C_g b = \boxed{\frac{\rho g H^2}{8} C_g b}$$

↳ (in kW)
in SI

$$\text{Watt} = \frac{\text{Joule}}{\text{sec}}$$

Power per unit crest width

" b

Wave Energy Converters (WEC)



wave crests (top view)

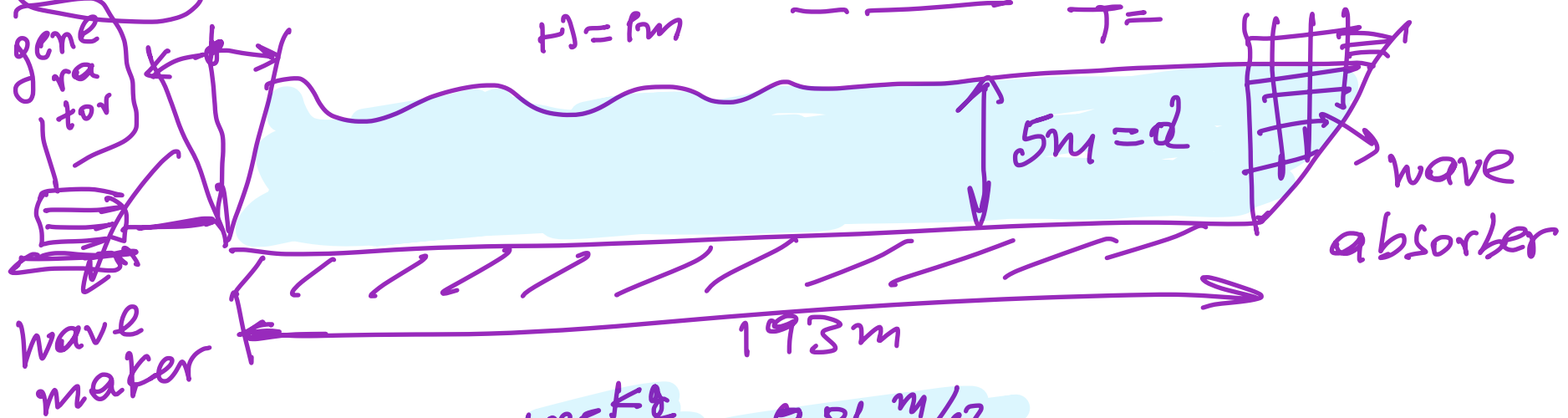
$$\bar{P} = \frac{\rho g H^2}{8} C_g$$

$$\boxed{P = \bar{P} \cdot b}$$

($\frac{\text{kW}}{\text{m}}$)
in SI

WAVE POWER/EXAMPLE

A sea-water wave tank at the U.S. Army Coastal Engineering Research Center is 193 m long, 4.57 m wide, and 5 m deep. Assume that the wave energy is fully absorbed at the opposite end of the wave generator. What power is required to generate 4-second waves which are 1m high, assuming that the wave generator is 40% efficient?



$$P_{\text{waves}} = \frac{\rho g H^2 C_g b}{8}$$

$\rho = 1,025 \frac{\text{kg}}{\text{m}^3}$
 $g = 9.81 \frac{\text{m}}{\text{s}^2}$
 $H = 1 \text{ m}$
 $b = 4.57 \text{ m}$

$$C_g = 1.56 \frac{\text{m}}{\text{s}} ; T = 4 \text{ sec} \Rightarrow L_0 = \frac{g T^2}{2\pi} = 24.88 \text{ m}$$

WAVE POWER/EXAMPLE

A sea-water wave tank at the U.S. Army Coastal Engineering Research Center is 193 m long, 4.57 m wide, and 5 m deep. Assume that the wave energy is fully absorbed at the opposite end of the wave generator. What power is required to generate 4-second waves which are 1m high, assuming that the wave generator is 40% efficient?

$$\rightarrow \frac{d}{L_0} = \frac{5}{24.88} = 0.2002 \xrightarrow[\text{C-1}]{\text{Table}} \frac{d}{L} = 0.2252 \Rightarrow$$

$$\Rightarrow \boxed{L} = \frac{d}{0.2252} = \boxed{22.2 \text{ m}}$$

$$\boxed{C} = \frac{L}{T} = \frac{22.2}{4} = \boxed{5.55 \frac{\text{m}}{\text{s}}}$$

$$\boxed{C_g} = \textcircled{n} C = 0.6675 \times 5.55 = \boxed{3.705 \frac{\text{m}}{\text{s}}}$$

From Table C-1

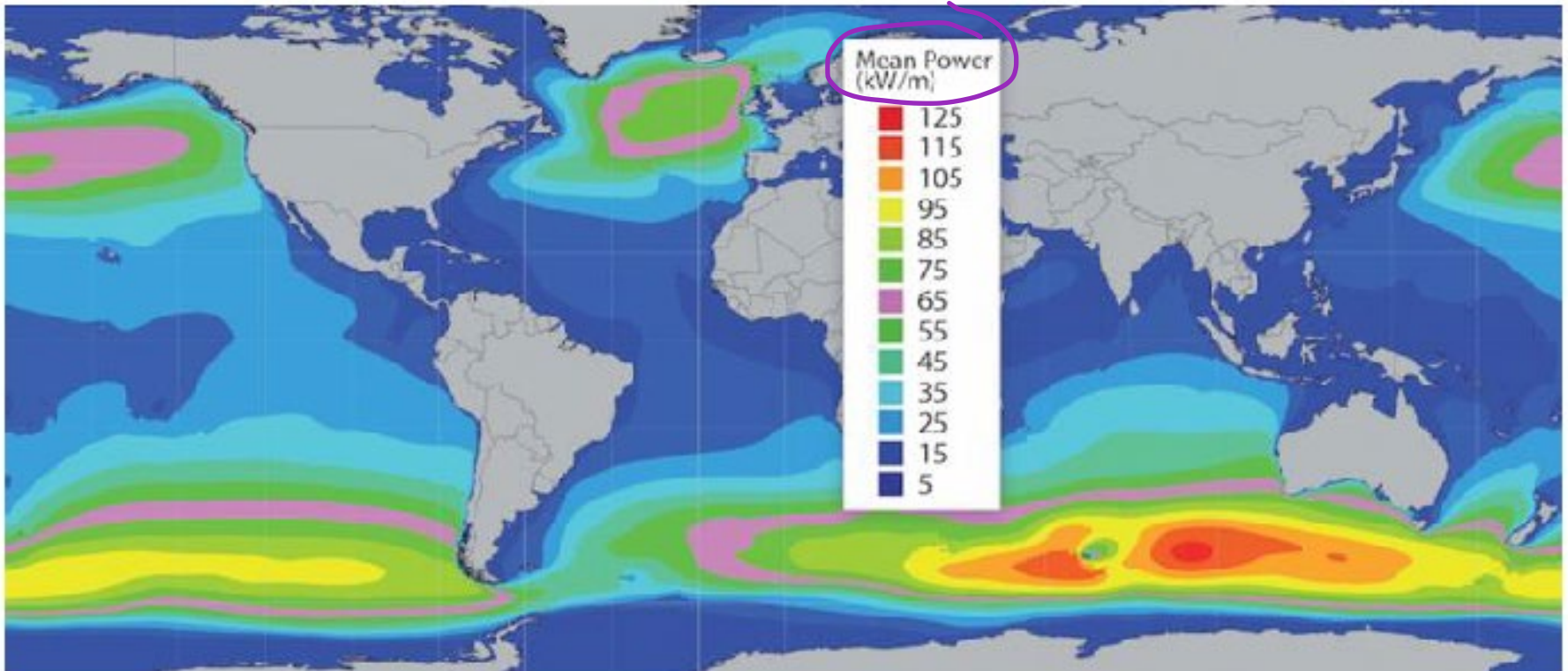
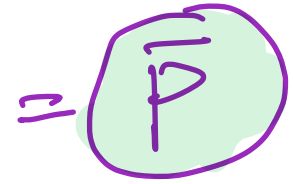
$$\text{with } \frac{d}{L_0} = 0.2002 \Rightarrow n = 0.6675$$

$$P_{\text{waves}} = \frac{1,025 \times 9.81 \times 1^2}{8} \times 3.705 \times 4.57 = 21,282 \text{ W} = 21.3 \text{ kW}$$

$$0.4 = \text{efficiency} = \frac{\text{useful power}}{\text{given power}} = \frac{P_{\text{waves}}}{P_{\text{gen}}}$$

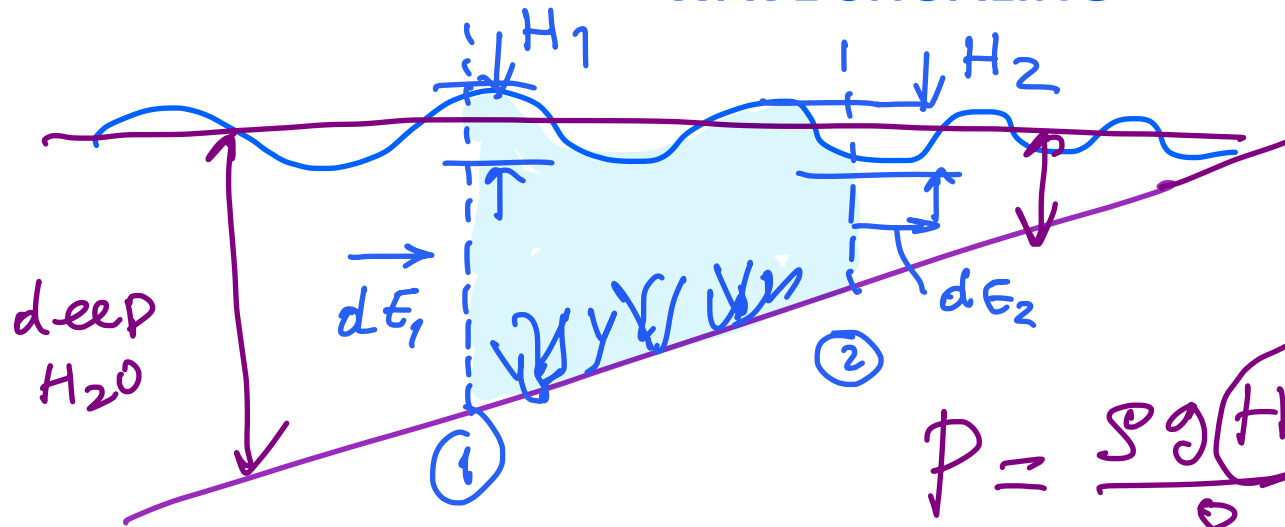
$$\Rightarrow P_{\text{generator}} = \frac{P_{\text{waves}}}{0.4} = \frac{21.3}{0.4} = 53.2 \text{ kW}$$

Mean Wave Power (KW/m)



Lewis, A., S. Estefen, J. Huckerby, W. Musial, T. Pontes, J. Torres-Martinez, 2011: Ocean Energy. In IPCC Special Report on Renewable Energy Sources and Climate Change Mitigation [O. Edenhofer, R. Pichs-Madruga, Y. Sokona, K. Seyboth, P. Matschoss, S. Kadner, T. Zwickel, P. Eickemeier, G. Hansen, S. Schlömer, C. von Stechow (eds)], Cambridge University Press. Figure 6.1

WAVE SHOALING



T (period) stays the same
 $L \downarrow$ and $C \downarrow$
as $d \downarrow$

$$P = \frac{\rho g H^2}{8} \cdot C_g \cdot b$$

$$\frac{dE_1}{dt} = \frac{dE_2}{dt} \Rightarrow P_1 = P_2$$

assumes
no
energy
losses!

$$\frac{\cancel{\rho} \cancel{g} H_1^2}{\cancel{8}} C_{g1} \cancel{b_1} = \frac{\cancel{\rho} \cancel{g} H_2^2}{\cancel{8}} C_{g2} \cancel{b_2}$$

$$C_{g1} H_1^2 = C_{g2} H_2^2 \leadsto \frac{H_2}{H_1} = \sqrt{\frac{C_{g1}}{C_{g2}}}$$

If energy losses as the wave propagates

WAVE SHOALING

from 1 $\rightarrow$ 2 then $P_2 = x P_1$ where $0 < x < 1$

For example if 10% energy losses then $P_2 = 0.9 P_1$

Special application

if ① $\rightarrow$ ② $\leftarrow$ deep H_2O

② $\rightarrow$ corresponds to depth d .

$$C_{g0} H_0^2 = C_g H^2$$

$$K_s = \frac{H}{H_0} = \sqrt{\frac{C_{g0}}{C_g}} = \sqrt{\frac{C_0}{2nC}}$$

$$C_{g0} = \frac{C_0}{2} \quad (\text{deep } H_2O)$$

$$C_g = nC$$

K_s $\rightarrow$ Shoaling coefficient

$\rightarrow$ relates H at certain depth to that in deep water, H_0 , in the absence of energy losses

WAVE SHOALING COEFFICIENT

shoaling coefficient K_s

Table C-1. Continued.

d/L_0	d/L	$2\pi d/L$	TANH $2\pi d/L$	SINH $2\pi d/L$	COSH $2\pi d/L$	H/H_0	K	$4\pi d/L$	SINH $4\pi d/L$	COSH $4\pi d/L$	n	C_G/C_0	M
.1500	.1833	1.152	.8183	1.424	1.740	.9133	.5748	2.303	4.954	5.054	.7325	.5994	7.369
.1510	.1841	1.157	.8200	1.433	1.747	.9133	.5723	2.314	5.007	5.106	.7311	.5994	7.339
.1520	.1850	1.162	.8217	1.442	1.755	.9132	.5699	2.324	5.061	5.159	.7296	.5995	7.309
.1530	.1858	1.167	.8234	1.451	1.762	.9132	.5675	2.335	5.115	5.212	.7282	.5996	7.279
.1540	.1866	1.173	.8250	1.460	1.770	.9132	.5651	2.345	5.169	5.265	.7268	.5996	7.250
.1550	.1875	1.178	.8267	1.469	1.777	.9131	.5627	2.356	5.225	5.320	.7254	.5997	7.221
.1560	.1883	1.183	.8284	1.479	1.785	.9130	.5602	2.366	5.283	5.376	.7240	.5998	7.191
.1570	.1891	1.188	.8301	1.488	1.793	.9129	.5577	2.377	5.339	5.432	.7226	.5999	7.162
.1580	.1900	1.194	.8317	1.498	1.801	.9130	.5552	2.387	5.398	5.490	.7212	.5998	7.134
.1590	.1908	1.199	.8333	1.507	1.809	.9130	.5528	2.398	5.454	5.544	.7198	.5998	7.107
.1600	.1917	1.204	.8349	1.517	1.817	.9130	.5504	2.408	5.513	5.603	.7184	.5998	7.079
.1610	.1925	1.209	.8365	1.527	1.825	.9130	.5480	2.419	5.571	5.660	.7171	.5998	7.052
.1620	.1933	1.215	.8381	1.536	1.833	.9130	.5456	2.429	5.630	5.718	.7157	.5998	7.026
.1630	.1941	1.220	.8396	1.546	1.841	.9130	.5432	2.440	5.690	5.777	.7144	.5998	7.000
.1640	.1950	1.225	.8411	1.555	1.849	.9130	.5409	2.450	5.751	5.837	.7130	.5998	6.975
.1650	.1958	1.230	.8427	1.565	1.857	.9131	.5385	2.461	5.813	5.898	.7117	.5997	6.949
.1660	.1966	1.235	.8442	1.574	1.865	.9132	.5362	2.471	5.874	5.959	.7103	.5996	6.924
.1670	.1975	1.240	.8457	1.584	1.873	.9132	.5339	2.482	5.938	6.021	.7090	.5996	6.900
.1680	.1983	1.246	.8472	1.594	1.882	.9133	.5315	2.492	6.003	6.085	.7076	.5995	6.876
.1690	.1992	1.251	.8486	1.604	1.890	.9133	.5291	2.503	6.066	6.148	.7063	.5994	6.853

WAVE SHOALING - EXAMPLE

(From Ex. Prob. 6 from SPM p2-27)

TOP VIEW

Shoreline

bottom contour

a) Find H at $d=3m$

wave crests

$d=2m$

$d=4m$

$d=6m$

L_0 (deep H₂O)
 H_0 (wave height)

$H_0 = 2m, T = 10sec$

$$L_0 = \frac{gT^2}{2\pi} = 156m$$

$$\frac{d}{L_0} = \frac{3}{156} = 0.01923 \xrightarrow[\text{C-1}]{\text{Table}} \frac{H}{H_0} = 1.237 = K_s \quad (H'_0 \equiv H_0)$$

WAVE SHOALING - EXAMPLE

$$\frac{H}{H_0} = 1.237 \leadsto \boxed{H = 1.237 \times (2\text{m}) = 2.474\text{m}}$$

- b) Determine the rate at which energy per unit crest width is transported towards the shore line.

They are asking for: $\bar{P} = \frac{8gH^2}{8} \cdot C_g$

$\bar{P}$ can be evaluated in deep water or at $d=3\text{m}$. However $\bar{P}_0 = \bar{P} \rightarrow$ at $d=3\text{m}$

$$\bar{P}_0 = \frac{8gH_0^2}{8} C_{g_0} = \frac{1.025 \times 9.81 \times (2\text{m})}{8} \cdot \frac{15.6}{2}$$

$$C_{g_0} = \frac{C_0}{2} = \frac{L_0}{T} \cdot \frac{1}{2} = \frac{156}{10} \cdot \frac{1}{2} = 15.6/2$$

$$\bar{P} = \bar{P}_0 = 39.2 \text{ kW/m}$$

In case there are 10% losses $\leftarrow$ due to friction with sea-floor or vegetation

$$P = (0.9)P_0$$

Note: In the solution of part (b) we could use $\bar{P} = \frac{\rho g H^2}{8} \cdot C_g$ at $d = 3\text{m}$

That would involve $C_g = n \cdot C$ with $C = \frac{L}{T}$. So we would need

to find $\frac{d}{L_0} \xrightarrow{C-1} \frac{d}{L} \rightarrow L \rightarrow C = \frac{L}{T}$
 $\left. \begin{array}{c} \xrightarrow{C-1} \\ \rightarrow n \end{array} \right\}$

$$C_g = n \frac{L}{T}$$

The answer would be the same, but determining $\bar{P}_0$ is easier

TSUNAMIS

Harbor

Wave

$L = 100 \text{ km}$ in $d = 4 \text{ km}$

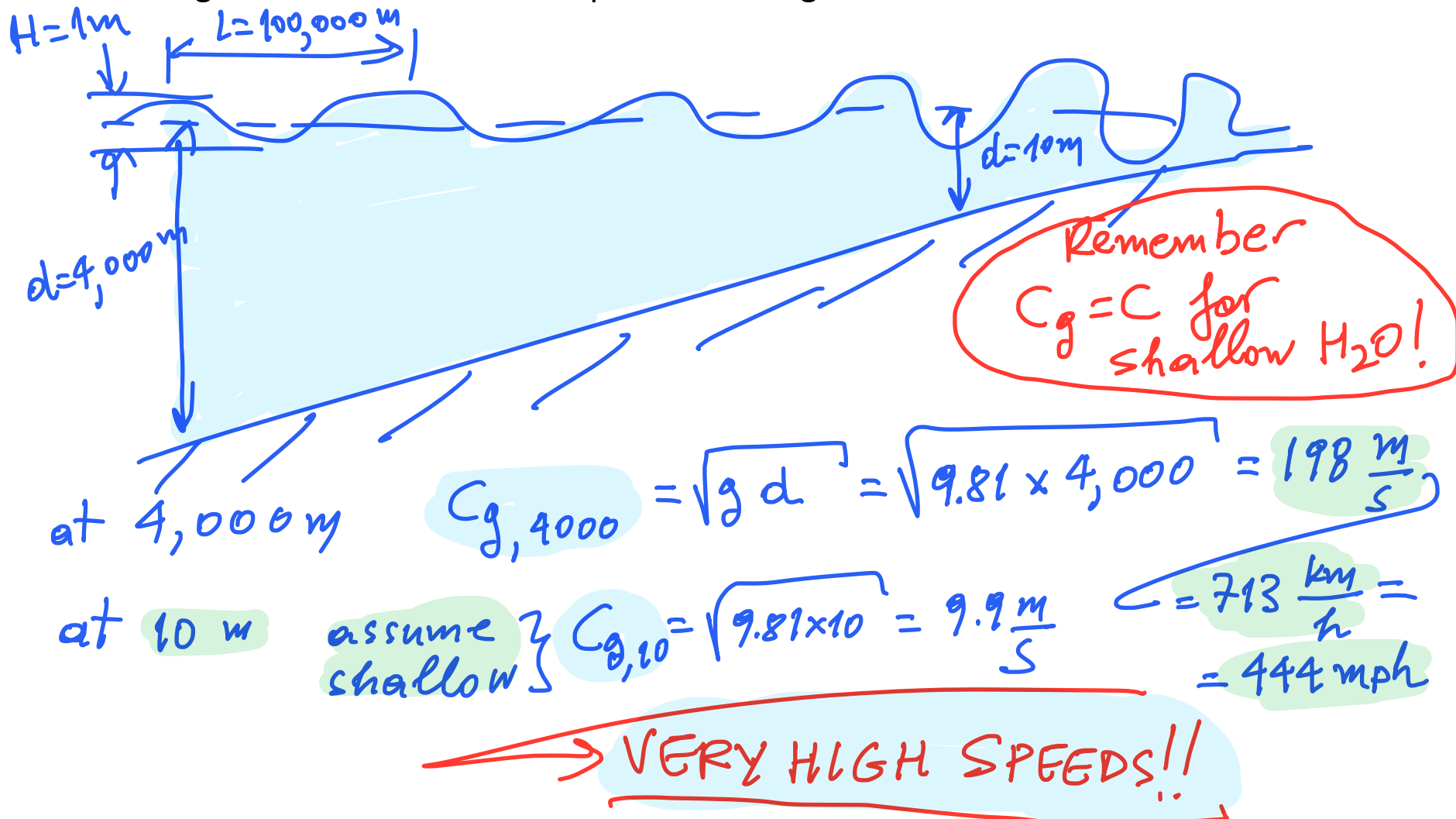
$\frac{d}{L} = 0.04 \Rightarrow \underline{\text{shallow H}_2\text{O}!!}$

In characterizing a wave as deep, transitional, or shallow

$\frac{d}{L}$ and NOT d is the critical parameter!

TSUNAMIS - EXAMPLE

An earthquake at a water depth of 4 km generates a tsunami with a length of 100 km and a height of 1m. Determine the speed of the front (in km/h and mph) of this tsunami at the depth of 4 km and at a depth of 10 m. What is the period (in minutes), the speed of its front, and the height of this tsunami at a depth of 10 m? Ignore refraction and reflection.



TSUNAMIS - EXAMPLE

An earthquake at a water depth of 4 km generates a tsunami with a length of 100 km and a height of 1m. Determine the speed of the front (in km/h and mph) of this tsunami at the depth of 4 km and at a depth of 10 m. What is the period (in minutes), the speed of its front, and the height of this tsunami at a depth of 10 m? Ignore refraction and reflection.

Find T from $d=4,000$

$$C_{g, 4000} = C_{4,000} = 198 \frac{\text{m}}{\text{s}} = \frac{L}{T} = \frac{100,000 \text{ m}}{T}$$

$$\Rightarrow T = \frac{100,000}{198} = 505 \text{ sec} = \underline{8.41 \text{ min}}$$

Now I can find L at $d=10 \text{ m}$

$$L = C_{10} \times T = 9.9 \times 500 = 5,000 \text{ m}$$

$$\text{At } d=10 \text{ m} \quad \frac{d}{L} = \frac{10}{5,000} = 2 \times 10^{-3} < 0.04$$

Shallow assumption
was correct!!

$$\bar{P}_{4,000} = \bar{P}_{10} \quad (\text{assuming no losses})$$

$$\frac{\cancel{8g} H_{4,000}^2}{\cancel{8}} \cdot C_{g,4000} = \frac{\cancel{8g} H_{10}^2}{\cancel{8}} \cdot C_{g,10}$$

$$H_{10} = \frac{H_{4,000}}{L=1m} \times \sqrt{\frac{C_{g,4000}}{C_{g,10}}} = 1m \times \sqrt{\frac{198}{9.9}} \Rightarrow$$

$H_{10} = 4.5m$

Significant wave height / /
magnification! -