7.5.4 The six-hour unit hydrograph of a watershed having a drainage area equal to $393 \mathrm{~km}^{2}$ is as follows:

| Time $(\mathrm{h})$ | 0 | 6 | 12 | 18 | 24 | 30 | 36 | 42 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Unit Hydrograph $\left(\mathrm{m}^{3} / \mathrm{s}^{*} \mathrm{~cm}\right)$ | 0 | 1.8 | 30.9 | 85.6 | 41.8 | 14.6 | 5.5 | 1.8 |

For a storm over the watershed having excess rainfall of 5 cm for the first six hours and 15 cm for the second six hours, compute the streamflow hydrograph, assuming a constant baseflow of $\mathbf{1 0 0}$ $\mathrm{m}^{3} / \mathrm{s}$.

| Area | $=393 \mathrm{~km} 2$ |
| ---: | :--- |
| Pe | $=r \mathrm{~cm}$ |
| Pe | $=15 \mathrm{~cm} \quad$ (first six hours) |
| (second six hours) |  |
| Baseflow | $=100 \mathrm{m3} / \mathrm{s}$ |


|  |  | Unit Hydrograph ordinates $\left(\mathrm{m} 3 / \mathrm{s}^{*} \mathrm{~cm}\right)$ |  |  |  |  |  |  |  |  |  | Direct |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Excess | 1 | 2 | 3 | 4 | 5 | 6 | 7 | Runoff | Streamflow |  |  |
| (h) | Precipitation $(\mathrm{cm})$ | 1.8 | 30.9 | 85.6 | 41.8 | 14.6 | 5.5 | 1.8 | $(\mathrm{~m} 3 / \mathrm{s})$ | $(\mathrm{m} 3 / \mathrm{s})$ |  |  |
| 6 | 5 | 9.0 |  |  |  |  |  |  | 9.0 | 109.0 |  |  |
| 12 | 15 | 27.0 | 154.5 |  |  |  |  |  | 181.5 | 281.5 |  |  |
| 18 |  |  | 463.5 | 428.0 |  |  |  |  | 891.5 | 991.5 |  |  |
| 24 |  |  |  | 1284.0 | 209.0 |  |  |  | 1493.0 | 1593.0 |  |  |
| 30 |  |  |  |  | 627.0 | 73.0 |  |  | 700.0 | 800.0 |  |  |
| 36 |  |  |  |  |  | 219.0 | 27.5 |  | 246.5 | 346.5 |  |  |
| 42 |  |  |  |  |  |  | 82.5 | 9.0 | 91.5 | 191.5 |  |  |
| 48 |  |  |  |  |  |  | 27.0 | 27.0 | 127.0 |  |  |  |


7.7.11 A triangular synthetic unit hydrograph developed by the Soil Conservation Service method has $q_{p}=2,900 c f s / i n, T_{p}=50 \mathrm{~min}$, and $t_{r}=10 \mathrm{~min}$. Compute the direct runoff hydrograph for a 20 -minute storm, having 0 .66in rainfall in the first 10 minutes and 1.70 in in the second 10 minutes. The rainfall loss rate is $\phi=0.6 \mathrm{in} / \mathrm{h}$ throughout the storm.
In this problem, what you need to do is to compute the triangular unit hydrograph by the SCS method, and then find the unit hydrograph flows at intervals of 10 minutes. Determine the excess rainfall amounts by subtracting $\phi=0.6 \mathrm{in} / \mathrm{hr}=0.1 \mathrm{in} / 10 \mathrm{~min}$ from the given rainfall values. Use the discrete convolution integral, Eq. (7.4.1), to compute the direct runoff hydrograph.
$q_{p}=2,900 c f s / i n$
$T_{p}=50 \mathrm{~min}$
$t_{b}=2.67 T_{p}$
$t_{b}=2.67(50 \mathrm{~min})$
$t_{b}=133.5 \mathrm{~min}$
Flow Rate $= \begin{cases}\frac{q_{p}}{T_{p}}(\text { time }) & \text { if } 0 \leq \text { time } \leq T_{p} \\ q_{p}-\frac{q_{p}}{1.67 T_{p}}\left(\text { time }-T_{p}\right) & \text { if } T_{p}<\text { time } \leq t_{b}\end{cases}$

| Time <br> $(\mathrm{min})$ | Flow <br> $(\mathrm{cfs} / \mathrm{in})$ |
| :---: | :---: |
| 0.0 | 0 |
| 10.0 | 580 |
| 20.0 | 1160 |
| 30.0 | 1740 |
| 40.0 | 2320 |
| 50.0 | 2900 |
| 60.0 | 2553 |
| 70.0 | 2205 |
| 80.0 | 1858 |
| 90.0 | 1511 |
| 100.0 | 1163 |
| 110.0 | 816 |
| 120.0 | 469 |
| 130.0 | 122 |
| 133.5 | 0 |



| $\begin{aligned} & \text { Time } \\ & (\mathrm{min}) \\ & \hline \end{aligned}$ | Rainfall <br> (in) | $\qquad$ | Unit Hydrigraph ordinates (cfs/in) |  |  |  |  |  |  |  |  |  |  |  |  | Direct <br> Runoff <br> (cfs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $1$$580$ | 2$1160$ | 3 <br> 1740 | 4$2320$ | 5 <br> 2900 | 6$2553$ | 7$2205$ | 8$1858$ | $9$$1511$ | $\begin{gathered} 10 \\ 1163 \\ \hline \end{gathered}$ | $11$$816$ | $12$$469$ | $13$$122$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 0.66 | 0.56 | 324.8 |  |  |  |  |  |  |  |  |  |  |  |  | 325 |
| 20 | 1.70 | 1.60 | 928.0 | 649.6 |  |  |  |  |  |  |  |  |  |  |  | 1578 |
| 30 |  |  |  | 1856.0 | 974.4 |  |  |  |  |  |  |  |  |  |  | 2830 |
| 40 |  |  |  |  | 2784.0 | 1299.2 |  |  |  |  |  |  |  |  |  | 4083 |
| 50 |  |  |  |  |  | 3712.0 | 1624.0 |  |  |  |  |  |  |  |  | 5336 |
| 60 |  |  |  |  |  |  | 4640.0 | 1429.5 |  |  |  |  |  |  |  | 6070 |
| 70 |  |  |  |  |  |  |  | 4084.3 | 1235.0 |  |  |  |  |  |  | 5319 |
| 80 |  |  |  |  |  |  |  |  | 3528.6 | 1040.5 |  |  |  |  |  | 4569 |
| 90 |  |  |  |  |  |  |  |  |  | 2972.9 | 846.0 |  |  |  |  | 3819 |
| 100 |  |  |  |  |  |  |  |  |  |  | 2417.2 | 651.5 |  |  |  | 3069 |
| 110 |  |  |  |  |  |  |  |  |  |  |  | 1861.6 | 457.1 |  |  | 2319 |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  | 1305.9 | 262.6 |  | 1568 |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  | 750.2 | 68.1 | 818 |
| 140 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 194.5 | 194 |



## 3. Exercise on "Introduction to HEC-HMS"

1. Verify with hand computation the amount of excess precipitation that results from a 2 inch rainfall in 1 hour falling on a basin with a curve number of 80 and $25 \%$ impervious cover.

The Results from HEC-HMS are shown in the following table.

| Date | Time | Precip <br> (IN) | Loss <br> (IN) | Excess <br> (IN) |
| :--- | :--- | :---: | :---: | :---: |
| 01Jan2012 | $00: 00$ |  |  |  |
| 01Jan2012 | $00: 06$ | 0.20 | 0.15 | 0.05 |
| 01Jan2012 | $00: 12$ | 0.20 | 0.15 | 0.05 |
| 01Jan2012 | $00: 18$ | 0.20 | 0.15 | 0.05 |
| 01Jan2012 | $00: 24$ | 0.20 | 0.13 | 0.07 |
| 01Jan2012 | $00: 30$ | 0.20 | 0.11 | 0.09 |
| 01Jan2012 | $00: 36$ | 0.20 | 0.10 | 0.10 |
| 01Jan2012 | $00: 42$ | 0.20 | 0.09 | 0.11 |
| 01Jan2012 | $00: 48$ | 0.20 | 0.08 | 0.12 |
| 01Jan2012 | $00: 54$ | 0.20 | 0.07 | 0.13 |
| 01Jan2012 | $01: 00$ | 0.20 | 0.06 | 0.14 |

Precipitation in 6 min intervals is: $\mathrm{P}=6 \min (2 \mathrm{in} / 60 \mathrm{~min})=0.2$ in. And $\mathrm{S}=\frac{1,000}{\mathrm{CN}}-10=$ $\frac{1,000}{80}-10=2.5 \mathrm{in}$. The initial abstraction is $\mathrm{I}_{\mathrm{a}}=0.2 \mathrm{~S}=0.2(2.5)=0.5 \mathrm{in}$. This means that precipitation for the first two periods and the half of the third period are absorbed as part of the losses.

Continuing Abstraction is computed with the equation: $F_{a}=S\left(P-I_{a}\right) /\left(P-I_{a}+S\right)$. Where, $I_{a}$ and $P$ are cumulative values of initial abstraction and precipitation respectively. And the Cumulative Precipitation in excess is computed as $P_{e}=P-I_{a}-F_{a}$. The losses are the difference between Precipitation and Precipitation in excess.

We consider $25 \%$ of terrain with impervious cover. The losses will be $75 \%$ of the original value. Precipitation in Excess is obtained subtracting the Losses from Precipitation. The values are shown in the following table; notice that they match the values from HEC-HMS.

| Time | Precip. <br> [in] | Cumul. <br> P. [in] | Cumul. Abst. [in] |  | Cumul. P. in excess [in] | P. in excess <br> [in] | $\begin{gathered} \text { Loss } \\ \text { [in] } \end{gathered}$ | 25\% impervious |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Loss |  |  | P. in excess |
|  |  |  | la | Fa |  |  |  | [in] | [in] |
| 0:00 |  | 0.00 |  |  |  |  |  |  |  |  |
| 0:06 | 0.20 | 0.20 | 0.20 | 0.00 | 0.00 | 0.00 | 0.20 | 0.15 | 0.05 |
| 0:12 | 0.20 | 0.40 | 0.40 | 0.00 | 0.00 | 0.00 | 0.20 | 0.15 | 0.05 |
| 0:18 | 0.20 | 0.60 | 0.50 | 0.10 | 0.00 | 0.00 | 0.20 | 0.15 | 0.05 |
| 0:24 | 0.20 | 0.80 | 0.50 | 0.27 | 0.03 | 0.03 | 0.17 | 0.13 | 0.07 |
| 0:30 | 0.20 | 1.00 | 0.50 | 0.42 | 0.08 | 0.05 | 0.15 | 0.11 | 0.09 |
| 0:36 | 0.20 | 1.20 | 0.50 | 0.55 | 0.15 | 0.07 | 0.13 | 0.10 | 0.10 |
| 0:42 | 0.20 | 1.40 | 0.50 | 0.66 | 0.24 | 0.09 | 0.11 | 0.09 | 0.11 |
| 0:48 | 0.20 | 1.60 | 0.50 | 0.76 | 0.34 | 0.10 | 0.10 | 0.08 | 0.12 |
| 0:54 | 0.20 | 1.80 | 0.50 | 0.86 | 0.44 | 0.11 | 0.09 | 0.07 | 0.13 |
| 1:00 | 0.20 | 2.00 | 0.50 | 0.94 | 0.56 | 0.12 | 0.08 | 0.06 | 0.14 |

2. Prepare a graph that shows the relation between the peak discharge and curve number for increments of the curve number of 10 from 60 to 90. Assume zero impervious cover and a lag time of 60 min .

For each curve number a simulation is run. The peak discharge can be accessed in the summary table.

| Curve <br> Number | Peak Discharge <br> (cfs) |
| :---: | ---: |
| 60 | 276 |
| 70 | 1,076 |
| 80 | 2,448 |
| 90 | 4,643 |


3. For a curve number of 80 , prepare a graph that shows the relation between the peak discharge and the \% impervious cover for impervious cover 0 to $50 \%$ in $10 \%$ increments. Assume a lag time of 60 min .

Similar to the previous point, for each impervious value a simulation is run. The peak discharge can be accessed in the summary table.

| Impervious <br> Cover (\%) | Peak <br> Discharge <br> (cfs) |
| :---: | ---: |
| 0 | 2,448 |
| 10 | 2,982 |
| 20 | 3,522 |
| 30 | 4,064 |
| 40 | 4,630 |
| 50 | 5,196 |


4. For a curve number of 80 and zero impervious cover, prepare a graph that shows the relation between peak discharge and lag time for lag times in the range 30 min to 90 min in 10 min increments.

Similar to the previous two points, for each lag time value a simulation is run. The peak discharge can be accessed in the summary table.

| Lag time <br> $(\mathrm{min})$ | Peak Discharge <br> $(\mathrm{cfs})$ |
| :---: | ---: |
| 30 | 4,115 |
| 40 | 3,388 |
| 50 | 2,860 |
| 60 | 2,448 |
| 70 | 2,150 |
| 80 | 1,904 |
| 90 | 1,712 |


5. How long ( min ) does it take the peak to traverse the reach? Change the slope to 0.0001 (typical of slopes in Houston). What effect does this have on the outflow?

The peak is 2441.1 cfs . The time can be 8acquired in the Time-series table.

| Time | Outflow <br> (CFS) |
| :--- | ---: |
| $0: 00$ | 0 |
| $0: 06$ | 0 |
| $0: 12$ | 0 |
| $0: 18$ | 0 |
| $0: 24$ | 0 |
| $0: 30$ | 0.1 |
| $0: 36$ | 0.1 |
| $0: 42$ | 0.2 |
| $0: 48$ | 0.2 |
| $0: 54$ | 0.7 |
| $1: 00$ | 11.6 |


| Time | Outflow <br> (CFS) |
| ---: | ---: |
| $1: 06$ | 102 |
| $1: 12$ | 313.5 |
| $1: 18$ | 631.8 |
| $1: 24$ | 1015 |
| $1: 30$ | 1408.4 |
| $1: 36$ | 1780.3 |
| $1: 42$ | 2097.8 |
| $1: 48$ | 2315.1 |
| $1: 54$ | 2426.3 |
| $2: 00$ | 2441.4 |
| $2: 06$ | 2380.5 |

The peak takes 18 minutes to transverse the reach. If we change the slope to 0.0001 (next table), the peak takes only 6 minutes but it magnitude its reduced significantly to 1267.2 cfs.

| Time | Outflow <br> (CFS) |
| ---: | ---: |
| $0: 00$ | 0 |
| $0: 06$ | 0 |
| $0: 12$ | 0 |
| $0: 18$ | 0 |
| $0: 24$ | 0 |
| $0: 30$ | 0 |
| $0: 36$ | 0 |
| $0: 42$ | 0 |
| $0: 48$ | 3.6 |
| $0: 54$ | 16.9 |
| $1: 00$ | 87.1 |


| Time | Outflow <br> (CFS) |
| ---: | ---: |
| $1: 06$ | 218.8 |
| $1: 12$ | 397.6 |
| $1: 18$ | 607.5 |
| $1: 24$ | 827.9 |
| $1: 30$ | 1022.1 |
| $1: 36$ | 1165 |
| $1: 42$ | 1251.5 |
| $1: 48$ | 1283.6 |
| $1: 54$ | $\mathbf{1 2 6 7 . 2}$ |
| $2: 00$ | 1208.3 |

6. By how much does Dam 7 reduce the outflow from the basin? Suppose that you change the rainfall from 2 inches in the first hour to 10 inches, with 5 inches in the first hour and 5 inches in the second hour (this is the "rain bomb" that happened in Tropical Storm Hermine). What is the outflow from the Routing Reach then? By how much does Dam-7 then reduce the outflow? Does water start going over the Emergency Spillway in this case?

The peak inflow in the reservoir is $2,441.4 \mathrm{cfs}$ and the outflow is 99.9 cfs . The flow is reduced in 96\%.

If we consider 5 inches of precipitation in the first hour and another 5 inches in the second hour, the peak outflow from the routing reach is $24,055.3 \mathrm{cfs}$. The outflow from the reservoir is $1,549.1 \mathrm{cfs}$. The flow is reduced in $94 \%$.

The peak storage is $3,780 \mathrm{AC}-\mathrm{FT}$, that correspond to an elevation of 831 m . The water starts going to emergency spillway at 829 ft ; the emergency spillway was used.

