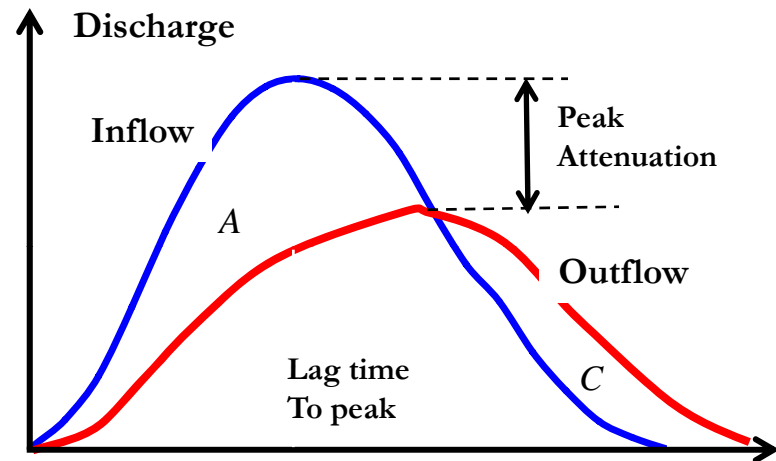
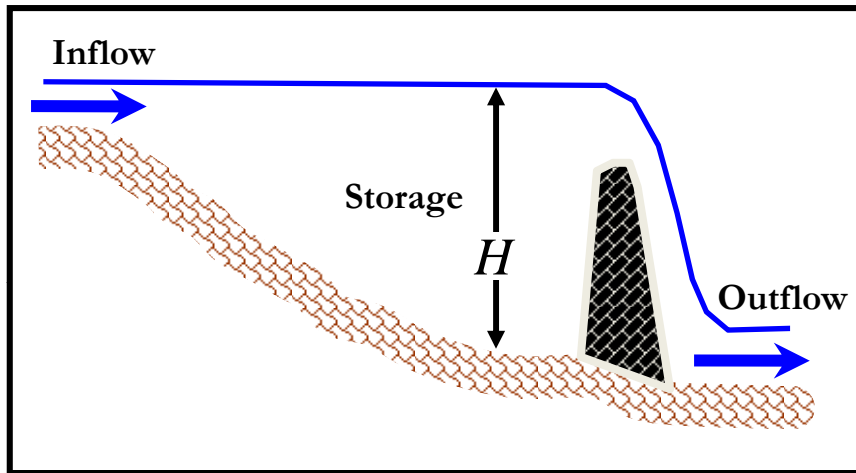


CE 374 K – Hydrology

Stream and Reservoir Routing

Daene C. McKinney

Reservoir Routing



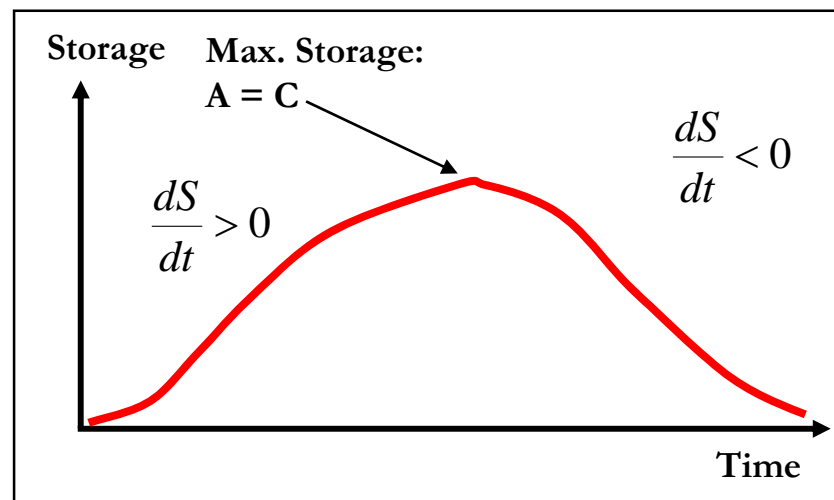
Inflow and outflow hydrographs for a small, level-surface reservoir

A: $I > O$, filling

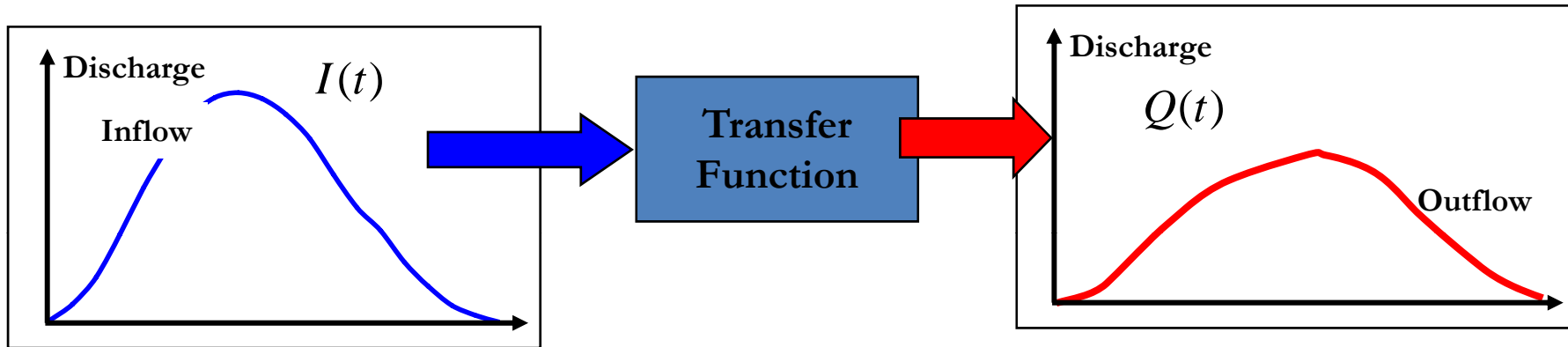
C: $I < O$, emptying

$$\frac{dS}{dt} = I(t) - Q(t)$$

$$Q(t) = f(H)$$



Hydrologic Routing



$$I(t) = \text{Inflow}$$

$$Q(t) = f[x, I(t)]$$

$$Q(t) = \text{Outflow}$$

Upstream
Hydrograph

Channel:
Characteristics: x
Routing Method: $f(\cdot)$

Downstream
Hydrograph

Input, output, storage
are related

$$\frac{dS}{dt} = I(t) - Q(t)$$

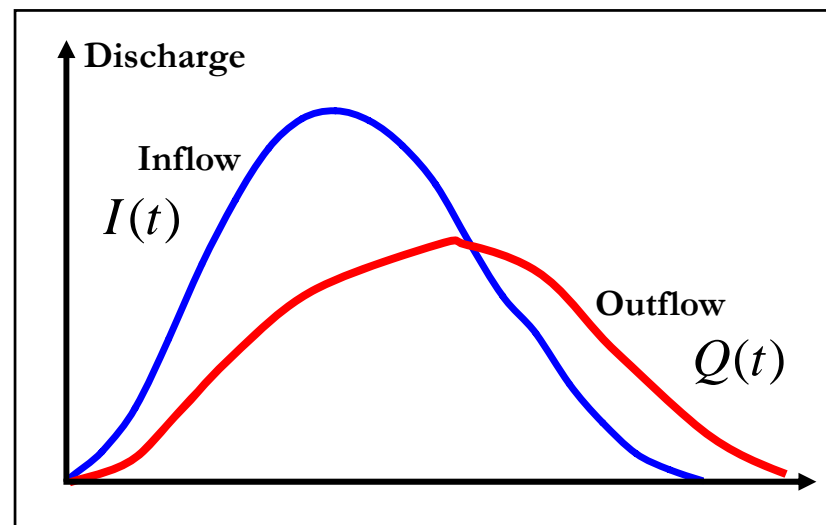
Storage function
is needed

$$S = f(I, Q)$$

Relations Between Discharge and Storage

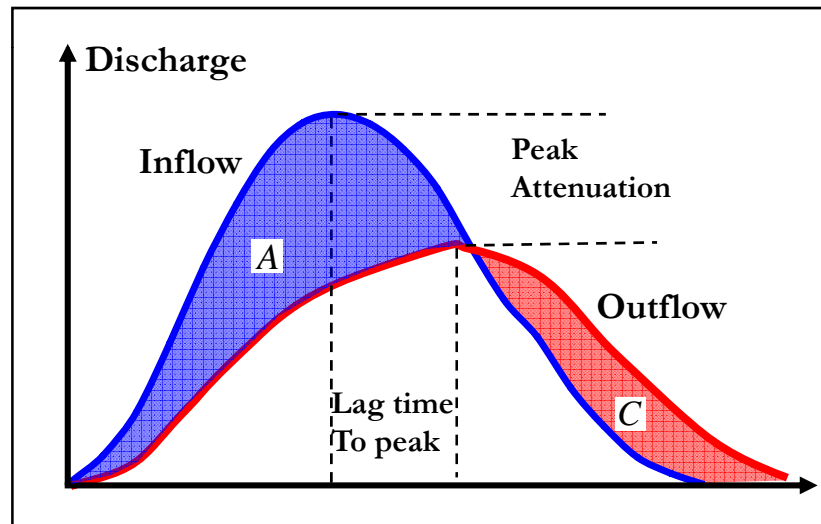
- Flow routing
 - Find a downstream hydrograph given an upstream hydrograph
 - Lumped or Distributed
 - Lumped $\frac{dS}{dt} = I(t) - Q(t)$
 - Storage function needed

$$S = f\left(I, \frac{dI}{dt}, \dots, Q, \frac{dQ}{dt}, \dots\right)$$



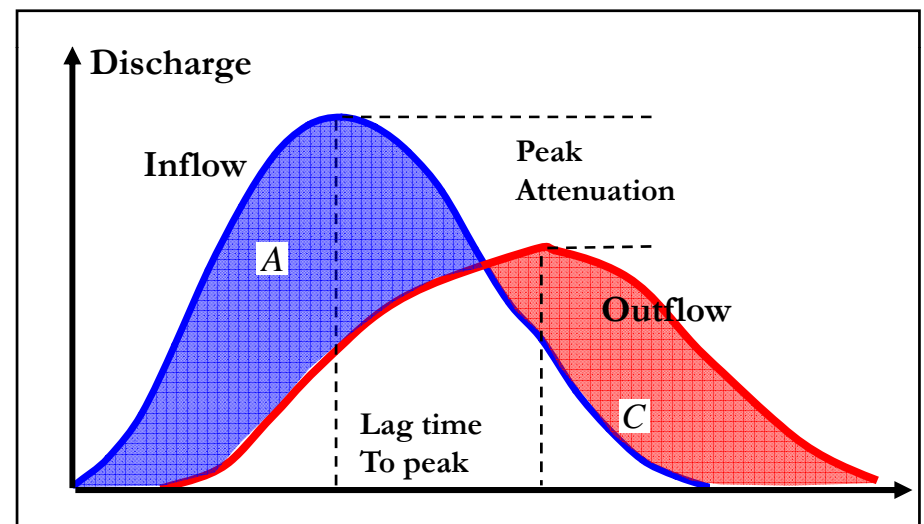
Transformation of Hydrographs: Redistribution and Translation

Redistribution



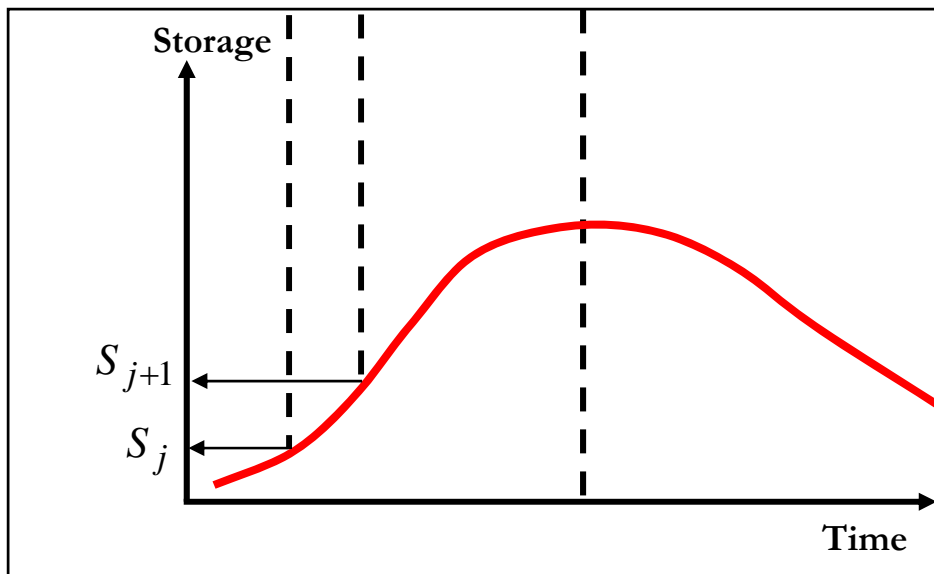
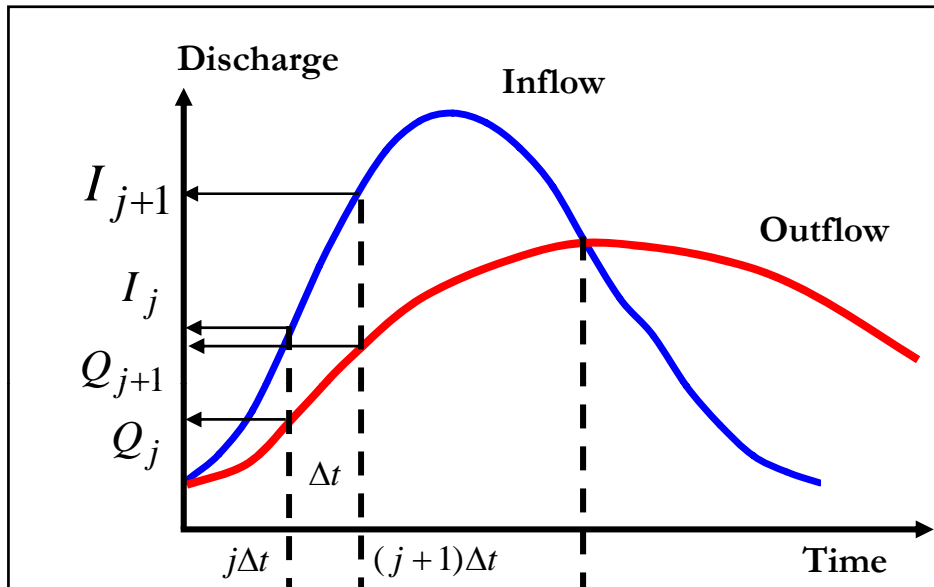
Reservoir Storage

Translation



Channel Storage

Reservoir Routing (Level Pool)



$$\frac{dS}{dt} = I(t) - Q(t)$$

$$S_{j+1} - S_j = \int_{j\Delta t}^{(j+1)\Delta t} I dt - \int_{j\Delta t}^{(j+1)\Delta t} Q dt$$

$$\frac{S_{j+1} - S_j}{\Delta t} = \frac{I_{j+1} + I_j}{2} - \frac{Q_{j+1} + Q_j}{2}$$

$$\frac{2S_{j+1}}{\Delta t} + Q_{j+1} = I_{j+1} + I_j + \frac{2S_j}{\Delta t} - Q_j$$

Unknown

Known

Need a function relating

$$\frac{2S}{\Delta t} + Q, \text{ and } Q$$

Level Pool Routing (Cont.)

$$\frac{2S_{j+1}}{\Delta t} + Q_{j+1} = I_{j+1} + I_j + \frac{2S_j}{\Delta t} - Q_j$$



Unknown



Known

Compute

$$\frac{2S_{j+1}}{\Delta t} + Q_{j+1}$$

From

$$\frac{2S}{\Delta t} + Q, \text{ and } Q$$

Then compute

$$Q_{j+1}$$

Then compute

$$\frac{2S_{j+1}}{\Delta t} - Q_{j+1} = \frac{2S_{j+1}}{\Delta t} + Q_{j+1} - 2Q_j$$

Level Pool Example

| H (ft) | A (ft ²) | S (ft ³) | 2S/Dt+Q (cfs) | Q (cfs) |
|--------|----------------------|----------------------|------------------|---------|
| 0 | 43,560 | 0 | 0 | 0 |
| 1 | 43,560 | 43,560 | 158 | 12.8 |
| 2 | 43,560 | 87,120 | 308.4 | 18 |
| 3 | 43,560 | 130,680 | 457.7 | 22.1 |
| 4 | 43,560 | 174,240 | 606.3 | 25.5 |
| 5 | 43,560 | 217,800 | 754.5 | 28.5 |
| 6 | 43,560 | 261,360 | 902.5 | 31.3 |
| 7 | 43,560 | 304,920 | 1050.2 | 33.8 |
| 8 | 43,560 | 348,480 | 1197.7 | 36.1 |
| 9 | 43,560 | 392,040 | 1345.1 | 38.3 |
| 10 | 43,560 | 435,600 | 1492.4 | 40.4 |

$$Q_{orifice} = C_d A_0 \sqrt{2gh}$$

Detention pond

Given:

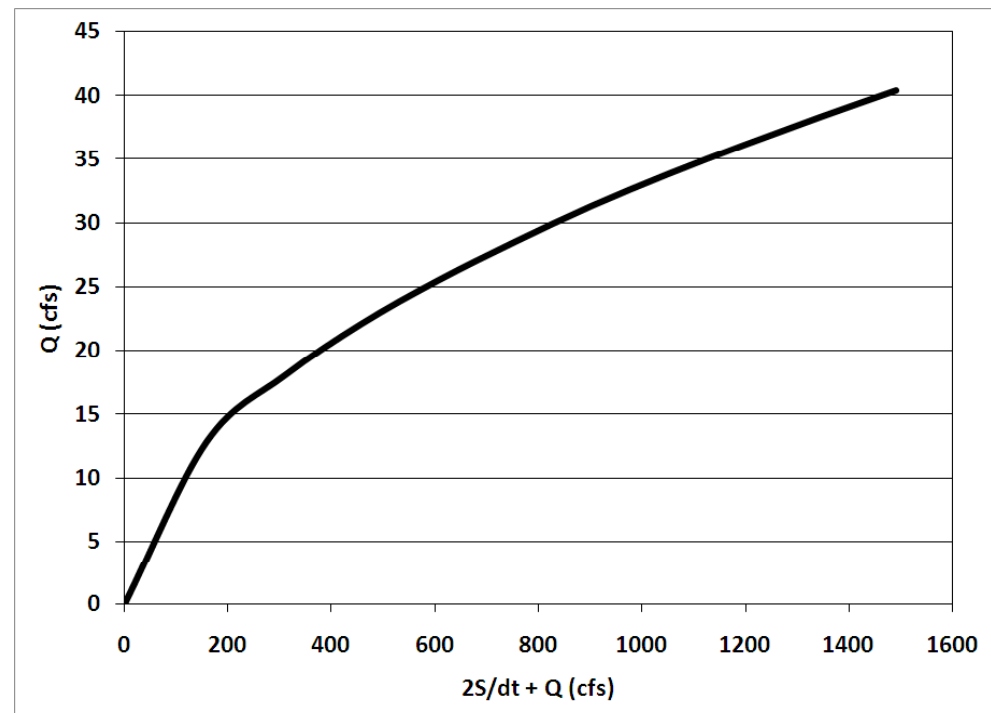
Area = 1 acre

Outlet = 18 inch diameter concrete pipe

C = 0.9

Find:

Outlet hydrograph



Level Pool Example (Cont.)

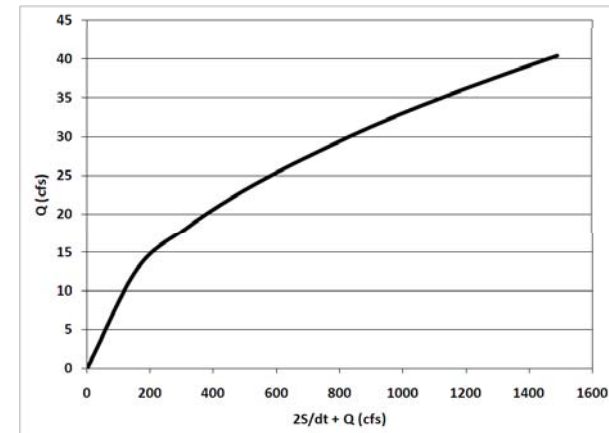
| Time (min) | I_j (cfs) | $I_j + I_{j+1}$ (cfs) | $\frac{2S_j}{dt} - Q_j$ (cfs) | $\frac{2S_{j+1}}{dt} + Q_{j+1}$ (cfs) | Q_j (cfs) |
|------------|-------------|-----------------------|-------------------------------|---------------------------------------|-------------|
| 0 | 0 | 0 | 0 | 0 | 0 |
| 10 | 20 | 20 | 11.8 | 20.0 | 4.1 |
| 20 | 40 | 60 | 54.6 | 71.8 | 8.6 |
| 30 | 60 | 100 | 129.0 | 154.6 | 12.8 |
| 40 | 50 | 110 | 207.2 | 239.0 | 15.9 |
| 50 | 40 | 90 | 261.6 | 297.2 | 17.8 |
| 60 | 30 | 70 | 294.2 | 331.6 | 18.7 |
| 70 | 20 | 50 | 306.2 | 344.2 | 19.0 |
| 80 | 10 | 30 | 299.2 | 336.2 | 18.5 |
| 90 | 0 | 10 | 273.2 | 309.2 | 18.0 |
| 100 | 0 | 0 | 239.2 | 273.2 | 17.0 |
| 110 | 0 | 0 | 207.4 | 239.2 | 15.9 |
| 120 | 0 | 0 | 178.0 | 207.4 | 14.7 |
| 130 | 0 | 0 | 151.0 | 178.0 | 13.5 |
| 140 | 0 | 0 | 126.4 | 151.0 | 12.3 |
| 150 | 0 | 0 | 104.0 | 126.4 | 11.2 |
| 160 | 0 | 0 | 83.8 | 104.0 | 10.1 |

$$\left(\frac{2S_{j+1}}{\Delta t} + Q_{j+1} \right) = (I_{j+1} + I_j) + \left(\frac{2S_j}{\Delta t} - Q_j \right)$$

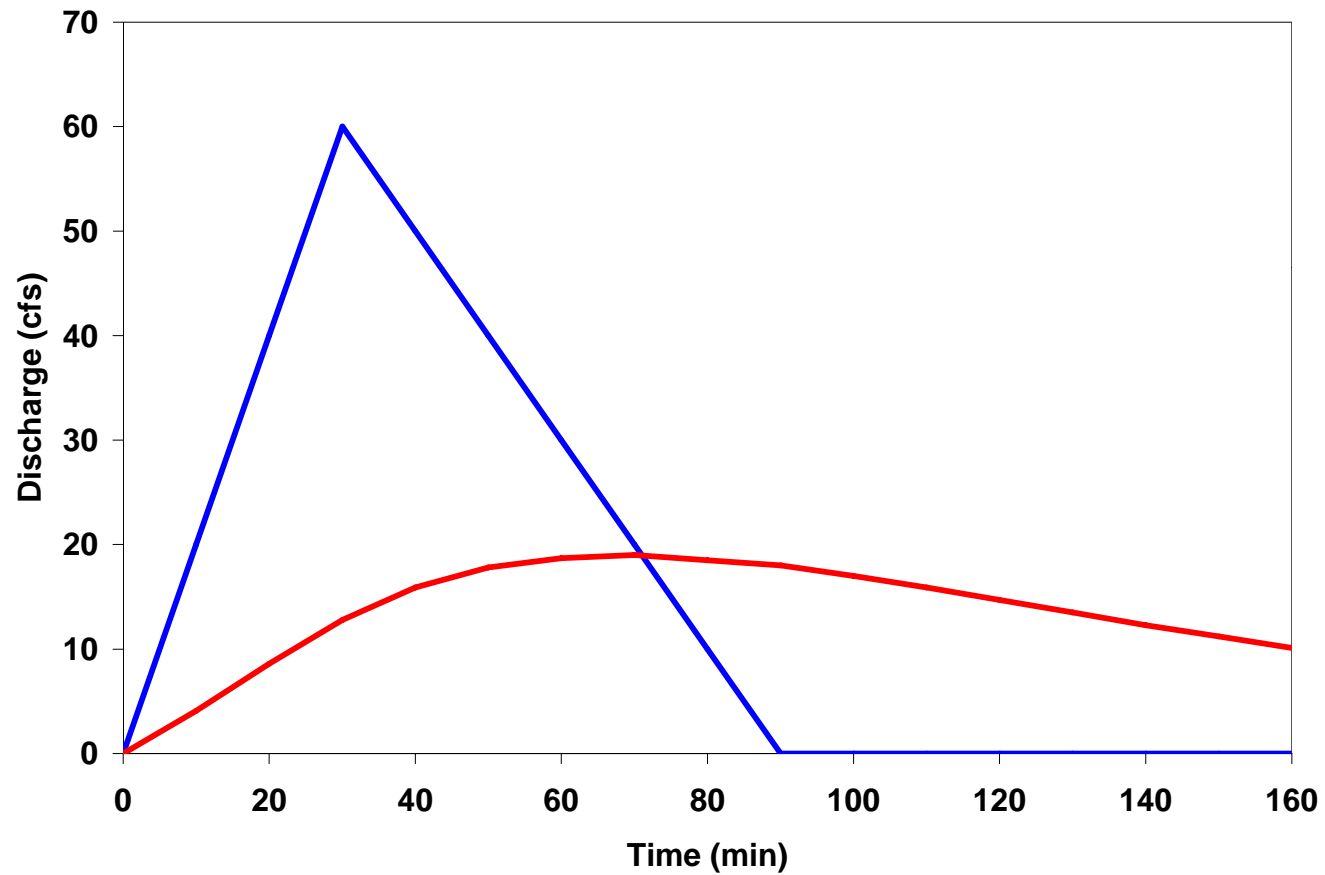
$$\left(\frac{2S_{j+1}}{\Delta t} + Q_{j+1} \right) \Rightarrow Q_j$$

$$\left(\frac{2S_j}{\Delta t} - Q_j \right) =$$

$$\left(\frac{2S_{j+1}}{\Delta t} + Q_{j+1} \right) - 2Q_j$$



Level Pool Example (Cont.)



Level Pool (Book Example)

Detention pond

Given:

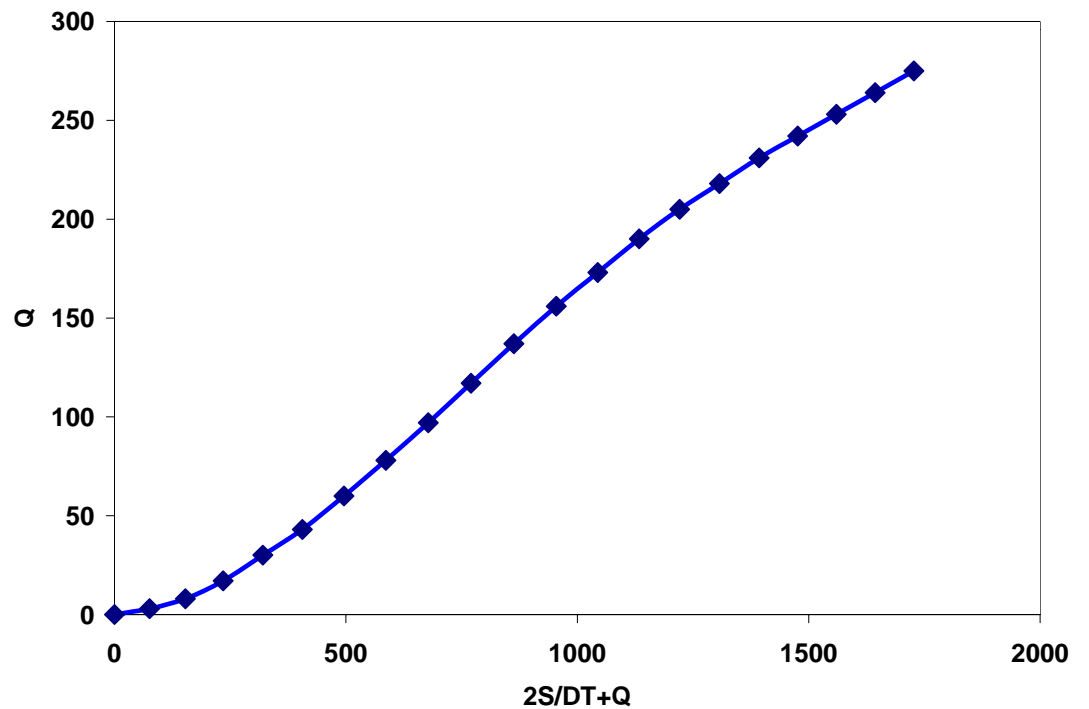
Area = 1 acre

Outlet = 5-ft diameter concrete pipe

Find:

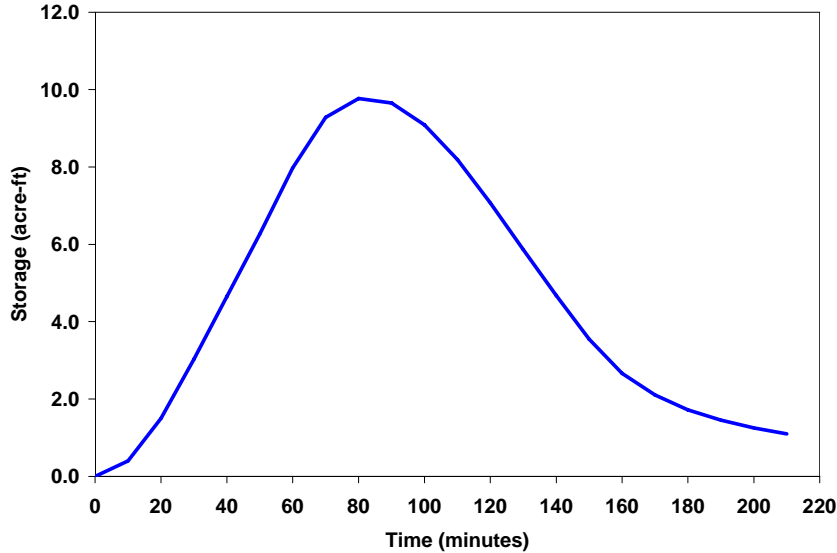
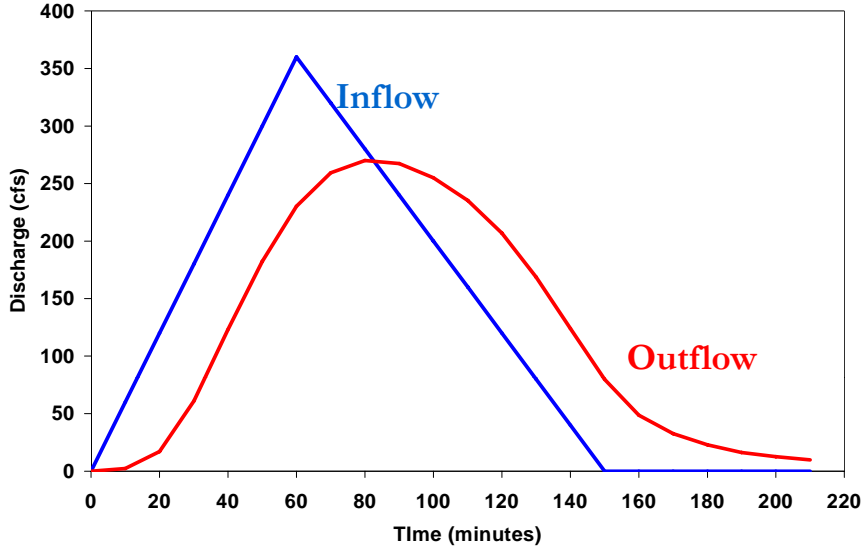
Outlet hydrograph

| H (ft) | Q (cfs) | S (ft ³) | $\frac{2S}{Dt} + Q$ (cfs) |
|-----------|------------|-------------------------|------------------------------|
| 0 | 0 | 0 | 0 |
| 0.5 | 3 | 21,780 | 76 |
| 1 | 8 | 43,560 | 153 |
| 1.5 | 17 | 65,340 | 235 |
| 2 | 30 | 87,120 | 320 |
| 2.5 | 43 | 108,900 | 406 |
| 3 | 60 | 130,680 | 496 |
| 3.5 | 78 | 152,460 | 586 |
| 4 | 97 | 174,240 | 678 |
| 4.5 | 117 | 196,020 | 770 |
| 5 | 137 | 217,800 | 863 |
| 5.5 | 156 | 239,580 | 955 |
| 6 | 173 | 261,360 | 1044 |
| 6.5 | 190 | 283,140 | 1134 |
| 7 | 205 | 304,920 | 1221 |
| 7.5 | 218 | 326,700 | 1307 |
| 8 | 231 | 348,480 | 1393 |
| 8.5 | 242 | 370,260 | 1476 |
| 9 | 253 | 392,040 | 1560 |
| 9.5 | 264 | 413,820 | 1643 |
| 10 | 275 | 435,600 | 1727 |



Level Pool Example (Cont.)

| Time (min) | Inflow (cfs) | I_j+I_{j+1} (cfs) | $2S_j/dt-Q_j$ (cfs) | $2S_{j+1}/dt-Q_{j+1}$ (cfs) | Outflow (cfs) |
|------------|--------------|---------------------|---------------------|-----------------------------|---------------|
| 0 | 0 | 0 | 0 | 0 | 0 |
| 10 | 60 | 60 | 55 | 60 | 2 |
| 20 | 120 | 180 | 201 | 235 | 17 |
| 30 | 180 | 300 | 379 | 501 | 61 |
| 40 | 240 | 420 | 552 | 799 | 123 |
| 50 | 300 | 540 | 728 | 1092 | 182 |
| 60 | 360 | 660 | 927 | 1388 | 230 |
| 70 | 320 | 680 | 1089 | 1607 | 259 |
| 80 | 280 | 600 | 1149 | 1689 | 270 |
| 90 | 240 | 520 | 1134 | 1669 | 267 |
| 100 | 200 | 440 | 1064 | 1574 | 255 |
| 110 | 160 | 360 | 954 | 1424 | 235 |
| 120 | 120 | 280 | 820 | 1234 | 207 |
| 130 | 80 | 200 | 683 | 1020 | 169 |
| 140 | 40 | 120 | 555 | 803 | 124 |
| 150 | 0 | 40 | 435 | 595 | 80 |
| 160 | 0 | 0 | 338 | 435 | 49 |
| 170 | 0 | 0 | 273 | 338 | 33 |
| 180 | 0 | 0 | 227 | 273 | 23 |
| 190 | 0 | 0 | 195 | 227 | 16 |
| 200 | 0 | 0 | 169 | 195 | 13 |
| 210 | 0 | 0 | 150 | 169 | 10 |



Hydrologic River Routing

Muskingum Method

- Wedge storage in reach

$$S_{Prism} = KQ$$

$$S_{Wedge} = KX(I - Q)$$

Advancing
Flood
Wave
 $I > Q$

K = travel time of peak through the reach

X = weight on inflow versus outflow

$X = 0 \rightarrow$ Reservoir, storage depends on outflow,

no wedge

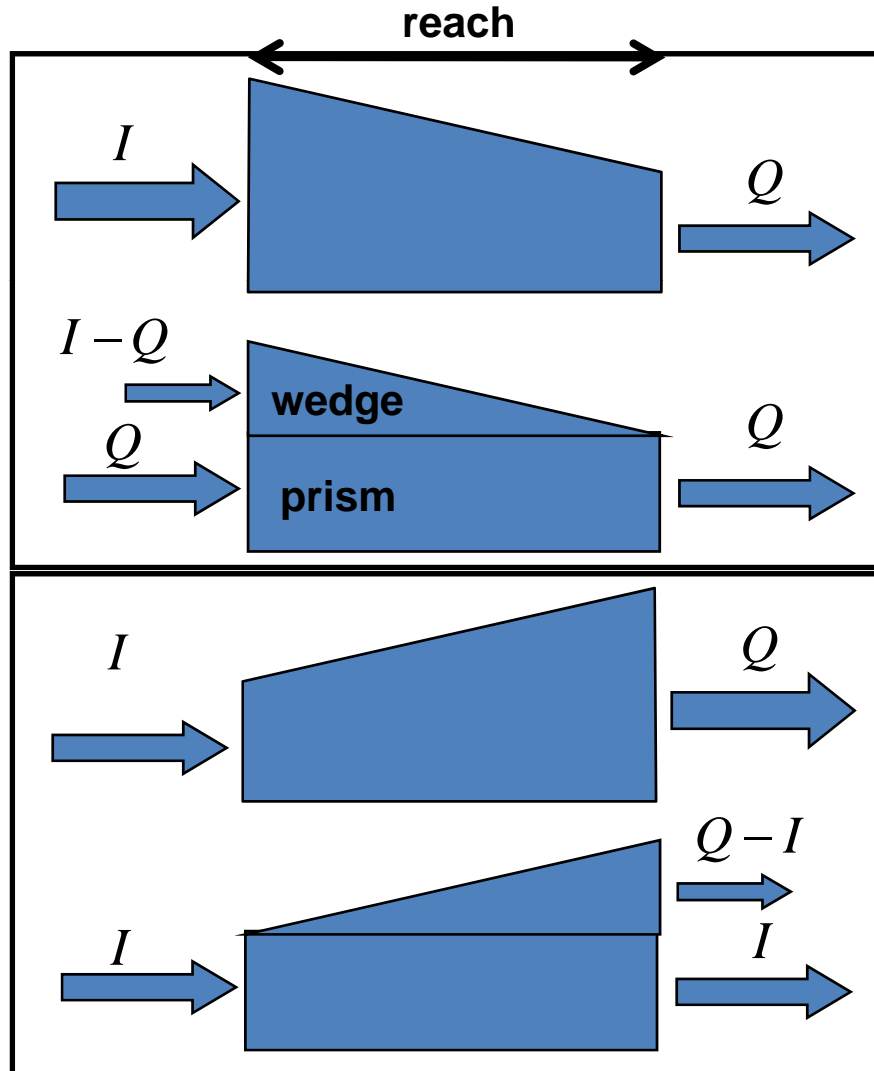
$X = 0.0 - 0.3 \rightarrow$ Natural stream

$$S = S_{wedge} + S_{prism}$$

$$= KQ + KX(I - Q)$$

$$S = K[XI + (1 - X)Q]$$

Receding
Flood
Wave
 $Q > I$



Muskingum Method (Cont.)

$$S = K[XI + (1 - X)Q]$$

$$S_{j+1} - S_j = K[XI_{j+1} + (1 - X)Q_{j+1}] - K[XI_j + (1 - X)Q_j]$$

Recall:

$$S_{j+1} - S_j = \frac{I_{j+1} + I_j}{2} \Delta t - \frac{Q_{j+1} + Q_j}{2} \Delta t$$

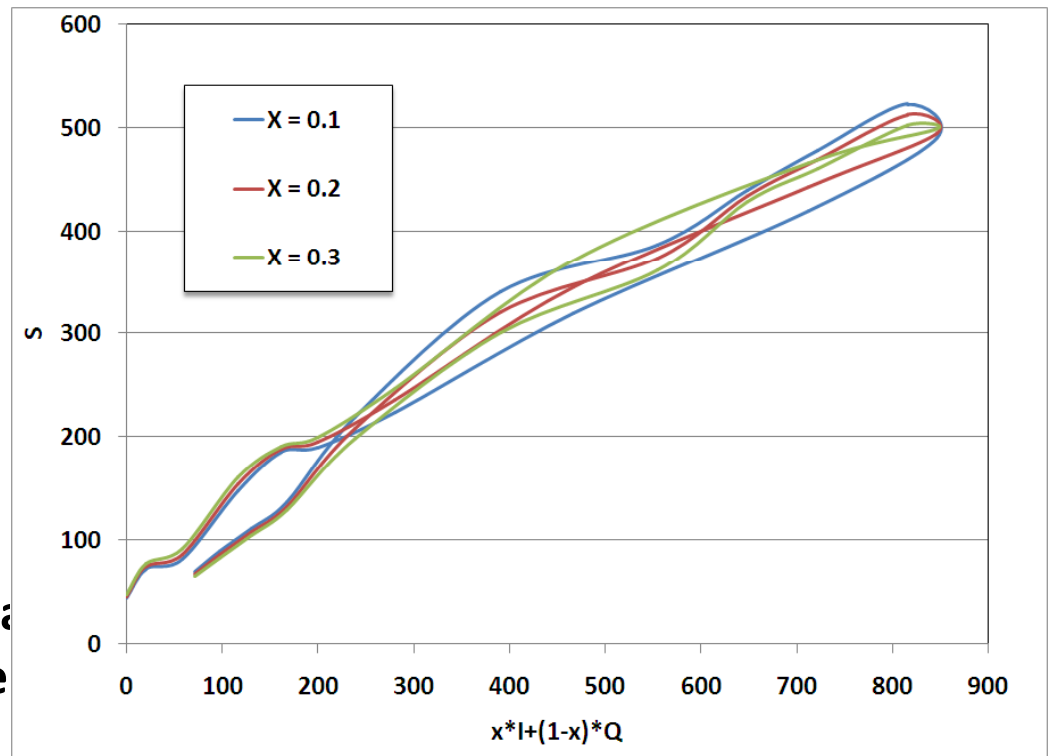
Combine:

$$Q_{j+1} = C_1 I_{j+1} + C_2 I_j + C_3 Q_j$$

$$C_1 = \frac{\Delta t - 2KX}{2K(1 - X) + \Delta t}$$
$$C_2 = \frac{\Delta t + 2KX}{2K(1 - X) + \Delta t}$$
$$C_3 = \frac{2K(1 - X) - \Delta t}{2K(1 - X) + \Delta t}$$

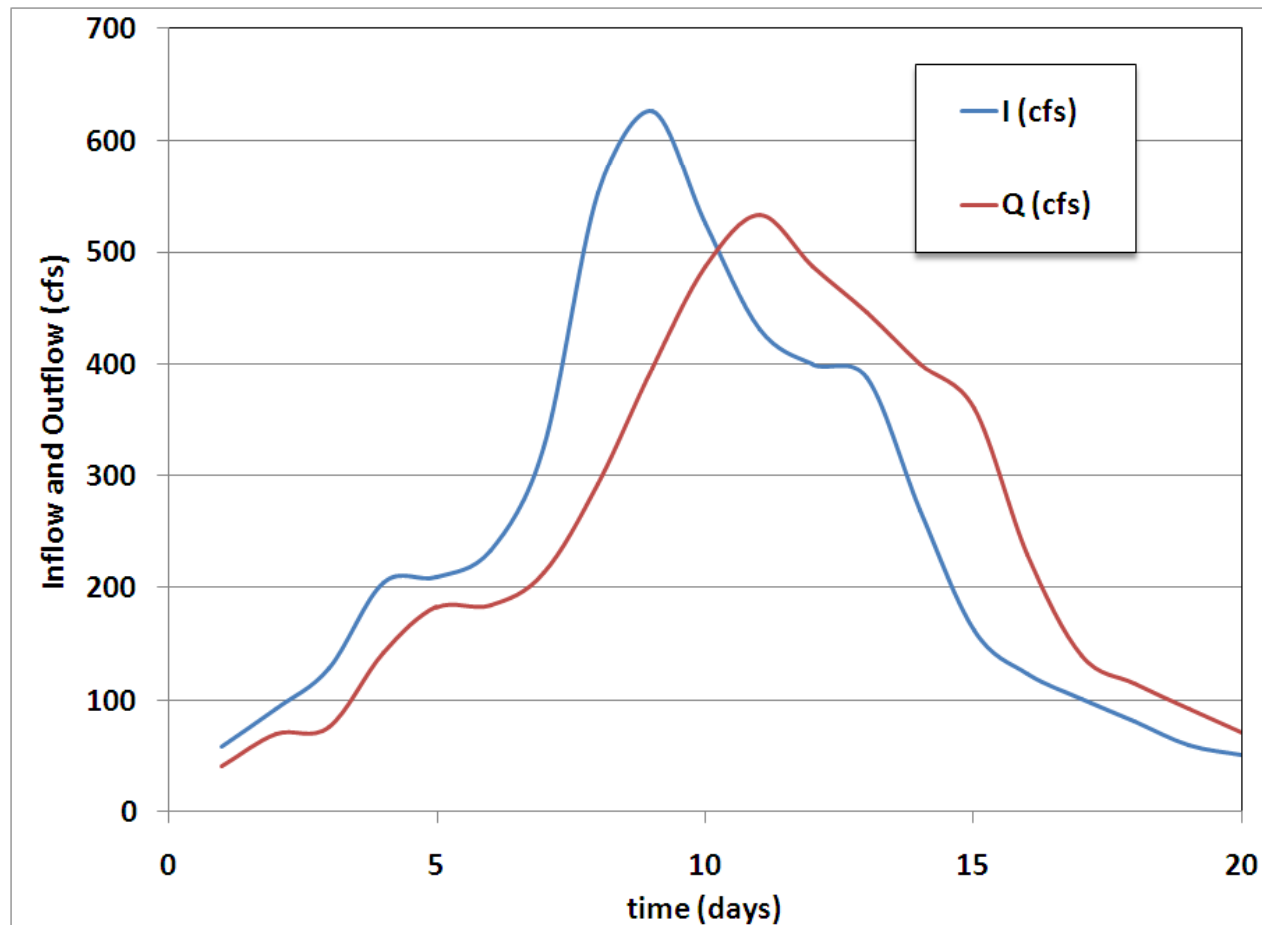
Muskingum Example

- Estimate K from observed inflow and outflow hydrographs
- Plot $[XI+(1-X)Q]$ vs. S
- For various values of X
- Choose the one which gives a loop closest to a straight line
- The Slope of this line is K



Muskingum Example

- River reach - Know inflow and outflow hydrographs
- Estimate Muskingum Parameters



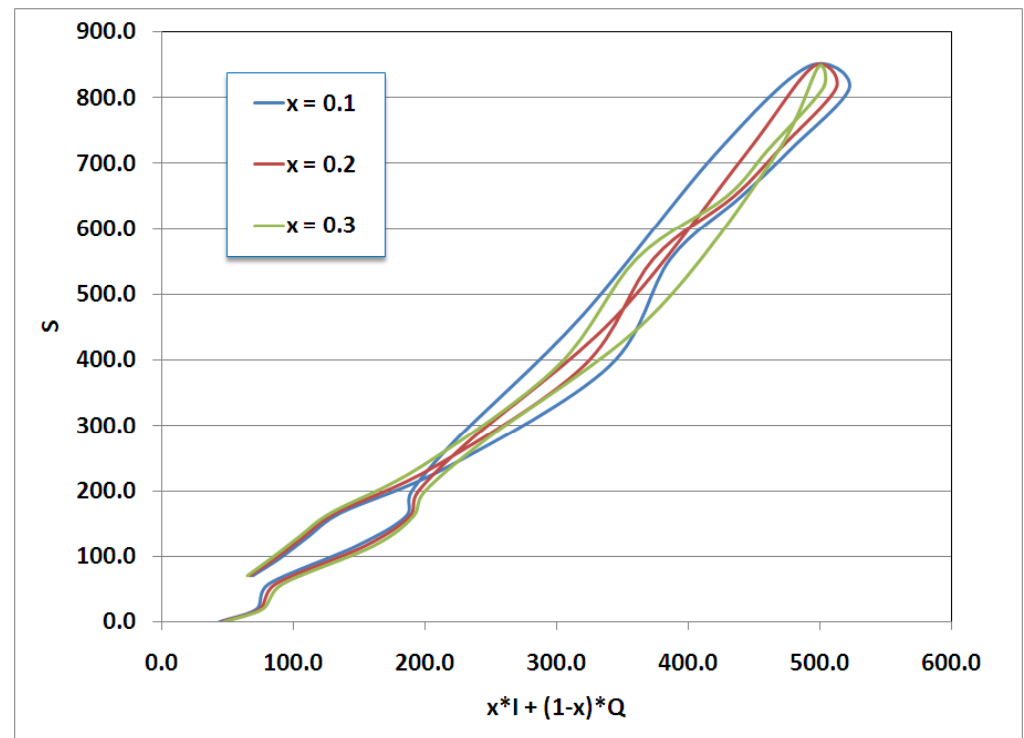
| Time (day) | I (cfs) | Q (cfs) |
|------------|---------|---------|
| 1 | 59 | 42 |
| 2 | 93 | 70 |
| 3 | 129 | 76 |
| 4 | 205 | 142 |
| 5 | 210 | 183 |
| 6 | 234 | 185 |
| 7 | 325 | 213 |
| 8 | 554 | 293 |
| 9 | 627 | 397 |
| 10 | 526 | 487 |
| 11 | 432 | 533 |
| 12 | 400 | 487 |
| 13 | 388 | 446 |
| 14 | 270 | 400 |
| 15 | 162 | 360 |
| 16 | 124 | 230 |
| 17 | 102 | 140 |
| 18 | 81 | 115 |
| 19 | 60 | 93 |
| 20 | 51 | 71 |

Muskingum Example (Cont.)

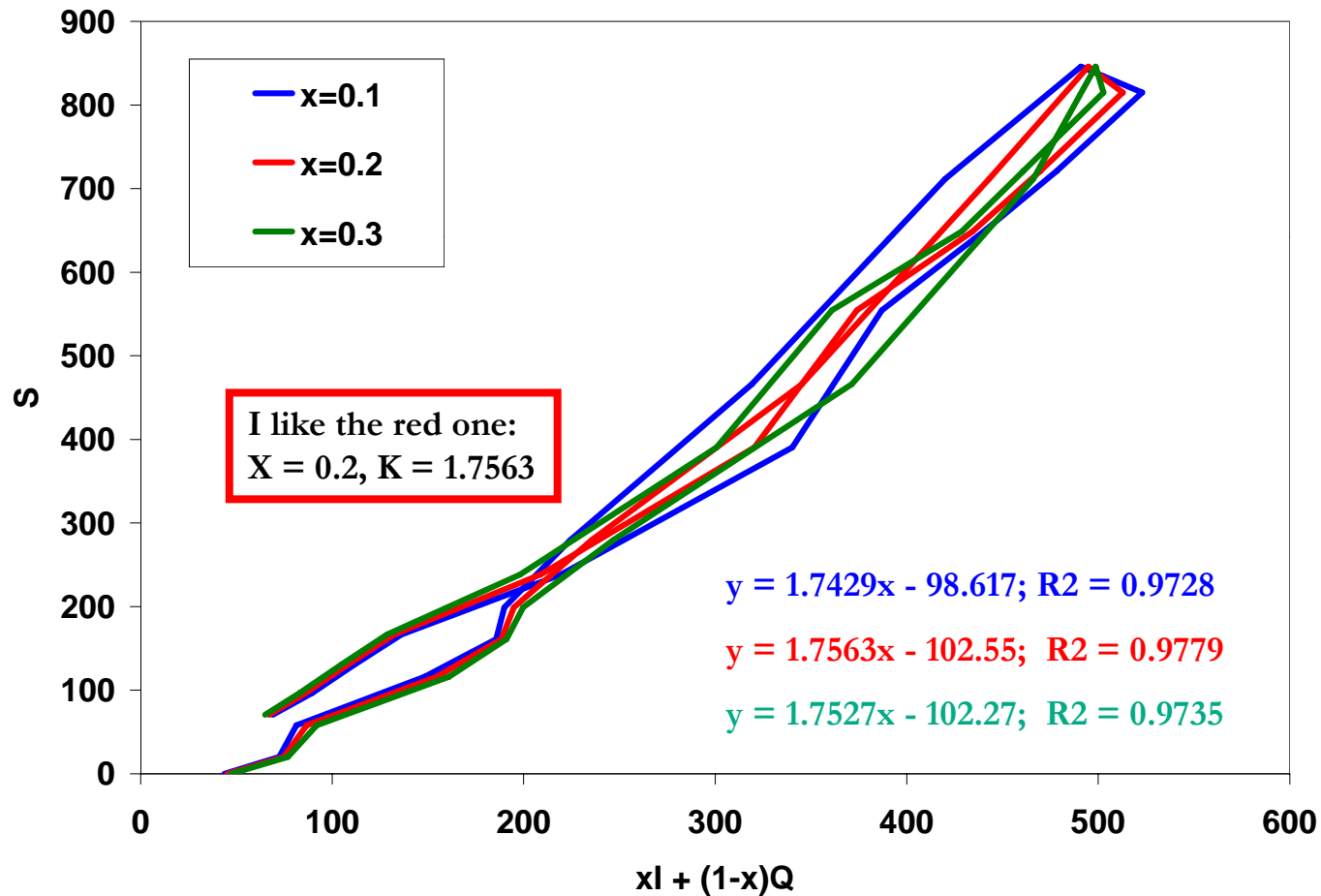
- Know inflow and outflow hydrograph
- Compute storage
- Compute $[XI+(1-X)Q]$ for various values of X

$$S_{j+1} = S_j + \frac{I_{j+1} + I_j}{2} \Delta t - \frac{Q_{j+1} + Q_j}{2} \Delta t$$

| Time t (day) | S S (ft3) | $xI+(1-x)Q$ X = 0.1 | $xI+(1-x)Q$ X = 0.2 | $xI+(1-x)Q$ X = 0.3 |
|-----------------|--------------|------------------------|------------------------|------------------------|
| 1 | 0 | 44 | 45 | 47 |
| 2 | 20 | 72 | 75 | 77 |
| 3 | 58 | 81 | 87 | 92 |
| 4 | 116 | 148 | 155 | 161 |
| 5 | 161 | 186 | 188 | 191 |
| 6 | 199 | 190 | 195 | 200 |
| 7 | 280 | 224 | 235 | 247 |
| 8 | 466 | 319 | 345 | 371 |
| 9 | 712 | 420 | 443 | 466 |
| 10 | 846 | 491 | 495 | 499 |
| 11 | 815 | 523 | 513 | 503 |
| 12 | 721 | 478 | 470 | 461 |
| 13 | 649 | 440 | 434 | 429 |
| 14 | 555 | 387 | 374 | 361 |
| 15 | 391 | 340 | 320 | 301 |
| 16 | 239 | 219 | 209 | 198 |
| 17 | 167 | 136 | 132 | 129 |
| 18 | 131 | 112 | 108 | 105 |
| 19 | 97 | 90 | 86 | 83 |
| 20 | 71 | 69 | 67 | 65 |



Muskingum Example (Cont.)



Muskingum Example (Cont.)

$$Q_{j+1} = C_1 I_{j+1} + C_2 I_j + C_3 Q_j$$

| t (day) | I (cfs) | C1*I _{j+1} | C2*I _j | C3*Q _j | Q (cfs) |
|---------|---------|---------------------|-------------------|-------------------|---------|
| 1 | 59 | 0 | 0 | 0.0 | 42 |
| 2 | 93 | 7.3 | 26.4 | 20.0 | 53.6 |
| 3 | 129 | 10.1 | 41.6 | 25.5 | 77.1 |
| 4 | 205 | 16.0 | 57.6 | 36.6 | 110.3 |
| 5 | 210 | 16.4 | 91.6 | 52.4 | 160.4 |
| 6 | 234 | 18.3 | 93.8 | 76.2 | 188.3 |
| 7 | 325 | 25.4 | 104.6 | 89.5 | 219.4 |
| 8 | 554 | 43.3 | 145.2 | 104.2 | 292.7 |
| 9 | 627 | 49.0 | 247.6 | 139.1 | 435.6 |
| 10 | 526 | 41.1 | 280.2 | 206.9 | 528.2 |
| 11 | 432 | 33.7 | 235.0 | 250.9 | 519.7 |
| 12 | 400 | 31.2 | 193.0 | 246.9 | 471.2 |
| 13 | 388 | 30.3 | 178.7 | 223.8 | 432.9 |
| 14 | 270 | 21.1 | 173.4 | 205.6 | 400.1 |
| 15 | 162 | 12.6 | 120.6 | 190.1 | 323.4 |
| 16 | 124 | 9.7 | 72.4 | 153.6 | 235.7 |
| 17 | 102 | 8.0 | 55.4 | 112.0 | 175.3 |
| 18 | 81 | 6.3 | 45.6 | 83.3 | 135.2 |
| 19 | 60 | 4.7 | 36.2 | 64.2 | 105.1 |
| 20 | 51 | 4.0 | 26.8 | 49.9 | 80.7 |

